Criticality Safety in the
Handling of Fissile Material
(Revision of SSG-27)

DS 516

DRAFT SPECIFIC SAFETY GUIDE
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1. INTRODUCTION

BACKGROUND

NUCLEAR CRITICALITY CAN THEORETICALLY

1.1 Criticality can be achieved under certain conditions by most fissionable nuclides belonging to the actinide elements. Some of these nuclides are also fissile, meaning that they are able to support a critical self-sustaining nuclear chain reaction in a thermalized ('slow') neutron energy flux, with neutrons of all energies, but predominantly with slow neutrons [1]. This Safety Guide thus addresses criticality safety for fissile material and also covers mixtures of fissile and other fissionable nuclides.

1.2 Nuclear facilities and activities containing fissile material, and activities in which fissile material is handled, are required to be managed in such a way as to ensure criticality safety in normal operation, an adequate margin of subcriticality under operational states and under conditions that are referred to as credible abnormal conditions or conditions included in the design basis accidents (or the equivalent) [1]. This requirement is also established in IAEA Safety Standards Series No. SSR-4, Safety of Nuclear Fuel Cycle Facilities [2]. This applies to large commercial facilities that involve handling of fissile material in the production of fresh nuclear facilities with the management of spent fuel and with radioactive waste containing fissile nuclides, including the handling, processing, use, storage and disposal of such waste. This requirement also applies to fuel fabrication, facilities handling irradiated nuclear fuel and research and development facilities in which fissile material is handled. These requirements in SSR-4 also apply to radioactive waste from nuclear fuel cycle facilities that contains fissile material.

1.3 Requirements for the transport of packages containing fissile material, are established in IAEA Safety Standards Series No. SSR-6 (Rev. 1), Regulations for the Safe Transport of Radioactive Material, 2018 Edition [3].

1.4 The subcriticality of a system depends on many parameters relating to the fissile material, including its mass, concentration, moderation, geometry, volume, enrichment, nuclide composition, chemical form, temperature, and density. Subcriticality is also affected by the presence of other materials

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1 Fissile nuclides are nuclides, in particular $^{233}\text{U}$, $^{235}\text{U}$, $^{239}\text{Pu}$ and $^{241}\text{Pu}$, that are able to support a self-sustaining nuclear chain reaction with neutrons of all energies, but predominantly with slow neutrons.

2 Fissile material refers to a material containing any of the fissile nuclides in sufficient proportion to enable a self-sustained nuclear chain reaction with slow (thermal) neutrons.
such as neutron moderators, neutron absorbers and, neutron reflectors, and dynamic effects (in particular, for fluids). Subcriticality can be ensured through the control of an individual parameter or a combination of parameters, for example, by limiting mass alone or by limiting both mass and moderation. Such parameters can be controlled by engineered and/or administrative measures.

**OBJECTIVE**

1.5 In this Safety Guide, the phrase ‘nuclide composition’ encompasses all the parameters inferred by the terms ‘enrichment’, ‘effective enrichment’, ‘plutonium vector’ and ‘isotopic composition’. Other terms used in this publication are as defined in the IAEA Safety Glossary [1].

1.6 This Safety Guide supersedes the 2014 version of SSG-27.

**OBJECTIVE**

1.7 The objective of this Safety Guide is to provide guidance and recommendations on meeting the relevant requirements for ensuring established in SSR-4 [2], and also in SSR-6 (Rev. 1) [3] (see para. 1.13), in respect of the following:

(a) Ensuring and demonstrating subcriticality and for planning the response under operational states and under conditions that are referred to as credible abnormal conditions or conditions included in the design basis;

(b) Estimating the credible consequences of a potential criticality accident. The guidance and recommendations are applicable for both regulatory bodies and operating organizations. This occurs.

1.8 Safety Guide—The recommendations on how criticality safety provided in this Safety Guide are also relevant to meet the requirements relating to criticality safety established in the following safety standards, including IAEA Safety Standards Nos GSR Part 4 (Rev. 1), Safety Assessment for Facilities and Activities [2], Management System for [3], GSR Part 2, Leadership and Management for Safety [5], GSR Part 5, Predisposal Management of Radioactive Waste [46], GSR Part 6, Decommissioning of Facilities Using Radioactive Material [5], Regulations for the Safe Transport of Radioactive Material [7], SSR-5, Disposal of Radioactive Waste [28], and GSR Part 7, Preparedness and

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The Safety Guide is intended for use by operating organizations, regulatory bodies and other organizations involved in ensuring criticality safety are defined in the IAEA Safety Glossary. Facilities and activities.

SCOPE

THE CRITICALITY SAFETY SCOPE

This Safety Guide applies to all facilities and activities that involve handling of fissile material, except those that are intentionally designed to be critical, for example a reactor core in a nuclear reactor, or a critical assembly. In this publication, ‘handling of fissile material’ refers to all activities involving fissile material including its processing, use, storage, movement (i.e. within the site) and transport (i.e. off the site), as well as the management of radioactive waste containing fissile material.

The recommendations provided in this Safety Guide cover criticality safety during normal operation, anticipated operational occurrences, states and during conditions, in design basis accidents that are referred to as credible abnormal conditions, from initial design, through commissioning, through operation, and through to decommissioning and . It also applies to the design, operation and post-closure of waste disposal—facilities. This Safety Guide also provides recommendations on planning the emergency response in case of a criticality accident.

The recommendations provided in this Safety Guide address: approaches to and criteria for ensuring subcriticality; identification of credible abnormal conditions; conducting criticality safety assessments; verification, benchmarking and validation of calculation methods; safety measures to ensure subcriticality, and management of criticality safety.

In cases where criticality safety is specifically addressed by regulations, for example, the transport of fissile material in accordance with SSR-6 (Rev. 1), this Safety Guide supplements but does not replace the recommendations and guidance provided in corresponding IAEA Safety Guides, for example IAEA Safety Standards Series No. SSG-26 (Rev. 1), Advisory Material for the IAEA Regulations for the Safe Transport of Radioactive Material (2018 Edition). This Safety Guide does not cover activities at defence related facilities.

The recommendations provided in this Safety Guide may be applied to operations that are intended to remain subcritical in nuclear power plants and research reactors, for example, the storage and handling of fresh fuel and spent fuel. The recommendations of this Safety Guide encompass approaches to and criteria for ensuring subcriticality, conducting criticality safety assessments, including
the use of data; specifying safety measures to ensure subcriticality; and the planned response to criticality accidents.

1.15 This Safety Guide consists of six sections and an Annex. Section 2 provides an introduction to recommendations on the processes factors that affect criticality safety and provides guidance for criticality safety specialists. It also provides an introduction to recommendations on the management system that should be in place, safety criteria subcritical limits and safety margins, and criteria for determining exemptions to certain criticality safety measures. Section 3 provides recommendations on the safety measures necessary for ensuring subcriticality criticality safety, especially the importance of implementing adequate safety measures, the factors affecting these safety measures, and the roles and responsibilities of those involved in implementing the safety measures. Section 4 provides recommendations on conducting criticality safety assessments, the role of deterministic and probabilistic approaches, and the process methodology by which the criticality safety assessment should be carried out. Section 5 provides recommendations on criticality safety practices in the various areas of conversion and enrichment, fuel fabrication, spent irradiated fuel operations prior to reprocessing or disposal, reprocessing, radioactive waste management (i.e. processing, storage and disposal) and decommissioning, transport of fissile material, and research and development laboratories. Section 6 provides recommendations on planning the response to a criticality accident and the basic responsibilities of those involved. In addition, it provides guidance on criticality detection and alarm systems.

1.16 The Annex provides a bibliography of sources of useful background information on criticality safety, covering methodology for criticality safety assessment, handbooks, computational methods, training and education, and operating experience.
2. **THE APPROACH TO ENSURING CRITICALITY SAFETY**

GENERAL

**GENERAL CONSIDERATIONS FOR ENSURING CRITICALITY SAFETY**

2.1. **Ensuring subcriticality in accordance with Requirements 38 and 66 of SSR-4** [2] is an essential component of criticality safety. Safety measures, both engineered measures and administrative measures (i.e. based on actions of operating personnel), should be identified, implemented, maintained and periodically reviewed (see para. 6.138 of SSR-4 [2]), ensure that facilities are operated, and activities are conducted within specified operational limits and conditions that ensure subcriticality. **These safety measures should be identified, implemented, maintained and periodically reviewed to ensure that operations and activities stay within defined safety limits (see para. 2.9)** during operational states and during credible abnormal conditions (see para. 2.3).

2.2. **Subcriticality** is generally ensured through the control of a limited set of macroscopic parameters such as mass, concentration, moderation, geometry, nuclide composition, enrichment, chemical form, temperature, density, and neutron reflection, interaction or absorption—neutron multiplication and dynamic effects (in particular for fluids). The determination of a system on the basis of values of limits for these parameters—parameters such as neutron fission cross-sections, capture cross-sections and scattering cross-sections for the system—is generally performed on the basis of the effective neutron multiplication factor\(^4\) \((k_{\text{eff}})\) of a system, for which nuclear data are needed. Because the effective neutron multiplication factor depends on a large number of variables upon which neutron multiplication depends, there are many examples of apparently ‘anomalous’ behaviour in which changes are counterintuitive. Some other parameters, like the delayed neutron fraction \((\beta_{\text{eff}})\), might also play a role in the safety assessment, if dynamic effects can occur, in particular for fluids in accident conditions.

2.3. The operational states and credible abnormal conditions that could lead to criticality conditions include the initiating events listed in the Appendix to SSR-4 [2]. The credible abnormal conditions should be determined on the basis of deterministic analysis complemented, where practicable, by probabilistic

\(^4\)The effective neutron multiplication factor is the ratio of the total number of neutrons produced by a fission chain reaction to the total number of neutrons lost by absorption and leakage. The system is: (a) critical if \(k_{\text{eff}} = 1\); (b) subcritical if \(k_{\text{eff}} < 1\); and (c) supercritical if \(k_{\text{eff}} > 1\). It is however noted that the effective multiplication factor might be defined also in different ways, for example through the concept of reactivity.
safety assessment. In the identification of credible abnormal conditions, the facility design and the characteristics of the activity as well as operating experience feedback should be considered (see also Refs. [11] and [12]).

2.4. In accordance with Requirement 13 of SSR-4 [2], items that are important for criticality safety are required to be identified and classified on the basis of their safety function and safety significance. This includes items providing engineered or administrative criticality safety measures such as items for the prevention of criticality accidents and for the mitigation of consequences of such accidents.

2.5. A graded approach is required be used in developing and implementing the approach to ensuring criticality safety of facilities or activities that involve handling of fissile material; see Requirement 11 of SSR-4 [2]. The application of a graded approach should be determined on the basis of the type of facility or activity and its potential risk. The application of a graded approach should not compromise safety. The graded approach should be applied to the following:

(a) The scope and level of detail of the criticality safety assessment;

(b) The methods and enveloping criticality events used in the criticality safety assessment;

(c) The design of criticality detection and alarm systems in which the effective neutron multiplication factor5 ($k_{eff}$) changes in ways that seem counterintuitive;

(d) The level of training and qualification of personnel involved in criticality safety;

(e) Emergency preparedness and response for criticality accidents;

(f) Administrative measures for criticality control.

Facility specific attributes that are required to be taken into account in the application of a graded approach are listed in para 6.29 of SSR-4 [2].

2.6. Safety measures and nuclear security measures should be planned and implemented in an integrated manner, and as far as possible in a complementary manner, so that security measures do not compromise safety, and safety measures do not compromise security. The implications of security measures, in particular access control, should be assessed with respect to their effect on criticality safety. The training programme on criticality safety should include the relevant aspects of nuclear security and of accounting for and control of nuclear material. Similarly, security personnel and those personnel responsible for accounting for and control of nuclear material should receive at least basic training on criticality safety.

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5 The effective neutron multiplication factor is the ratio of the total number of neutrons produced by a fission chain reaction to the total number of neutrons lost by absorption and leakage. The system is: (a) critical if $k_{eff} = 1$; (b) subcritical if $k_{eff} < 1$; and (c) supercritical if $k_{eff} > 1$. 
2.2.7. Feedback of operating experience, including awareness of the previous anomalies known to date and accidents, should be used to contribute to ensuring criticality safety. Information on the causes and consequences of important anomalies that have been observed in criticality safety is provided in Refs. [12]–[15]. Events relating to criticality safety should be analysed and included in the operating experience programme. Requirements for feedback from operating experience for all facilities and activities are established in para. 6.7 of GSR Part 2 [5] and, for nuclear fuel cycle facilities, in Requirement 73 of SSR-4 [2]. Further recommendations are provided in IAEA Safety Standards Series No. SSG-50, Operating Experience Feedback for Nuclear Installations [16].

SAFETY CRITERIA AND SAFETY MARGINS

SUBCRITICAL LIMITS AND SAFETY MARGINS

2.3.8. Subcritical limits should be derived on the basis of one type or both of criteria the following:

(a) Safety criteria based on the subcritical value of $k_{\text{eff}}$ for the system under analysis;

(b) Safety criteria based on the critical value $k_{\text{eff}}$ of less than one. A set of one or more macroscopic control parameters, such as whose values, individually or in combination, for the system under analysis correspond to a $k_{\text{eff}}$ of less than one. Examples of such control parameters are mass, volume, concentration, geometry, moderation, geometry, nuclide composition, chemical form, temperature, density, and neutron reflection, interaction, composition and density, or absorption and dynamic effects (in particular for fluids), and with account taken of neutron production, leakage, scattering and absorption.

2.4. Safety margins should be applied to determine the criticality safety limits. Acceptance criteria should be defined, and it should be demonstrated that these criteria will not be exceeded. Furthermore, the upper bound of the uncertainty and sensitivity analysis of $k_{\text{eff}}$-calculations (see para. 2.10) should not exceed the acceptance criteria. Subcriticality implies a value of $k_{\text{eff}}$ of less than one and/or of a control parameter whose value is below its critical value. In this context, ‘below’ is used in the sense that the control parameter remains on the safe side of corresponds to a $k_{\text{eff}}$ of less than one. Paragraph 6.21 and Requirement 17 of SSR-4 [2] require the critical value use of conservative margins for design.

2.5. Consideration should be given to the uncertainties associated with the calculation of $k_{\text{eff}}$ when applying safety margins to $k_{\text{eff}}$ (relative to 1) and/or to a control parameter (relative to the critical value). Alternatively, consideration should be given to uncertainty in the calculation of other control parameters.

The critical value is that value of a control parameter that would result in the system no longer being reliably known to be subcritical.
parameters when applying safety margins to their corresponding critical values. This should include for example the possibility of any bias, and/or bias uncertainty in the calculation method, and the sensitivity with respect of parameter values to changes in the control parameter or $k_{\text{eff}}$. The relationship between $k_{\text{eff}}$ and other parameters may might be significantly non-linear.

2.11. In accordance with Requirement 38 of SSR-4 [2], the subcriticality of the design is required to be demonstrated in a full criticality safety assessment\(^7\). The criticality safety assessment should define criticality safety limits and, in turn, operational limits and conditions for criticality safety, which should be expressed in terms of the process parameters affecting the reactivity characteristics of a system. These parameters include mass, concentration, moderation, geometry, nuclide composition, chemical form, temperature, density, and neutron reflection, interaction or absorption and dynamic effects (in particular for fluids). The parameters quoted in limits and conditions should be expressed in terms that can readily be understood, such as enrichment, packaging rules and moisture or moderator material limit or restriction.

2.12. The operational limits and conditions specified for the facility or activity should be lower or equal to the criticality safety limits and should be suitable for being monitored and controlled. Sufficient and appropriate safety measures should be put in place applied to detect and intercept react to deviations from normal operation before any criticality safety limit is exceeded. Uncertainties in measurement, instruments, administrative errors and sensor delay should also be considered. Alternatively, design features should be put in place to prevent effectively criticality being achieved. This should also be demonstrated in the criticality safety assessment. Operational limits and conditions are often expressed in terms of process parameters, for example, when assessing the appropriateness of safety measures.

**EXEMPTION CRITERIA FOR FISSILE MASS AND MODERATOR CONTENT, CONCENTRATION, ACIDITY, LIQUID FLOW RATES AND TEMPERATURE MATERIAL**

**EXEMPTIONS**

2.6.2.13. In some cases, the amount of fissile material may be so low, or the nuclide composition may be such, that a full criticality safety assessment is not be justified. Exemption criteria, if not specified by the regulatory body, should be developed by the operating organization, reviewed by the management of the operating organization and then agreed with by the regulatory body, as appropriate. A useful starting point is the exception criteria applied to the classification of transport packages para.

\(^7\) Except where the quantity of fissile material involved is so low or the isotopic composition is such that it meets exemption criteria (see paras 2.13–2.16) specified by, or agreed with, the regulatory body.
containing fissile material in para. 417 (a), (b), (e) in conjunction with para. 570 of SSR-6 (Rev. 1) [3].

2.7.2.14. The primary approach in seeking exemption should be to demonstrate that the inherent features of the fissile material itself are sufficient to ensure subcriticality. The secondary approach should be to demonstrate that the maximum amounts of fissile nuclides involved are so far below minimum critical values that no specific safety measures are necessary to ensure subcriticality in normal operation, anticipated operational occurrences or design basis accidents (or the equivalent).

2.8.2.15. Modifications to facilities and/or activities should are required to be evaluated before being implemented, to determine whether the bases for the exemption remain valid: see paras 6.141 and 9.83 of SSR-4 [2].

MANAGEMENT SYSTEM

2.16. The basis for meeting exemption criteria should be documented and justified.

MANAGEMENT SYSTEM FOR CRITICALITY SAFETY

2.1. A documented management system that integrates the safety, health, environmental, security, quality, and human and organizational factors with criticality safety measures should be carried out within a clearly defined management system. The IAEA requirements and recommendations for implemented with adequate resources, in accordance with Requirement 4 of SSR-4 [2]. As part of the management system, management should be established in Ref. [3] and provided, early in Ref. [12–16], respectively.

2.2. In the context of criticality safety, the following items should be taken into account for the implementation of a management system:

2.9.2.17. Management should establish a comprehensive design stage a criticality safety programme should be established and put into effect by the operating organization, to ensure that safety measures for ensuring subcriticality are specified, implemented, monitored, audited, documented and periodically reviewed throughout the entire lifetime of the facility or the duration of the activity.

- Management should ensure that a plan for corrective action is established, as required, is implemented and is updated when necessary.

2.19. The management system (which is required to cover all items, services and processes important to safety: see para. 4.8 of SSR-4 [2]) should include activities in relation to criticality safety, thereby providing confidence that they are performed correctly. In determining how the management system for criticality safety is to be applied, a graded approach on the basis of the relative importance to safety of each item or process is required to be used: see Requirement 7 of GSR Part 2 [5]. The management system is required to support the development and maintenance of a strong safety culture, including in all aspects of criticality safety: see Requirement 12 of GSR Part 2 [5].

2.20. The management system should ensure that the facility or activity achieves the necessary level of criticality safety, as derived from: regulatory requirements; the design requirements and assumptions; the safety analysis report, and operational limits and conditions, including administrative requirements.

2.21. In accordance with paras 4.15–4.23 of SSR-4 [2], the management system should address the following functional areas:

(a) Management responsibility, which includes the support and commitment of management necessary to achieve the objectives of the operating organization.

(b) Resource management, which includes the measures necessary to ensure that the resources essential to the implementation of strategy and the achievement of the objectives of the operating organization are identified and made available.

(c) Process implementation, which includes the activities and tasks necessary to achieve the goals of the organization.

(d) Measurement, assessment and improvement, which provide an indication of the effectiveness of management processes and work performance compared with objectives or benchmarks; it is through measurement and assessment that opportunities for improvement are identified.

Management responsibility

2.22. The prime responsibility for safety, including criticality safety, rests with the operating organization. In accordance with para. 4.11 of GSR Part 2 [5], the documentation of the management system for criticality safety is required to include the following:

(a) A description of the organizational structure;

(b) Functional responsibilities;

(c) Levels of authority.

The documentation should describe the interactions among the individuals managing, performing and
assessing the adequacy of the criticality safety programme and activities. The documentation should also cover other management measures, including planning, scheduling and resource allocation (see para. 9.8 of SSR-4 [2]).

2.23. There should be a designated person (or persons) who is responsible and accountable for criticality safety, including, as appropriate, the following:

(a) Developing and documenting all aspects of criticality safety assessment.
(b) Monitoring the performance of activities and processes.
(c) Ensuring that personnel are adequately trained.
(d) Operating a system for keeping records that ensures control of performance and verification of activities that are important to criticality safety. The record keeping system should provide for the identification, approval, review, filing, retrieval, and disposal of records.


“the management system shall include provisions for ensuring effective communication and clear assignment of responsibilities, in which accountabilities are unambiguously assigned to individual roles within the organization and to suppliers, to ensure that processes and activities important to safety are controlled and performed in a manner that ensures that safety objectives are achieved.”

Arrangements for empowering relevant personnel to stop unsafe operations should also be made.

2.25. The operating organization is required to ensure that criticality safety assessments and analyses are conducted, documented and updated; see Requirement 24 and paragraph 4.65 of GSR Part 4 (Rev. 1) [4] and Requirement 5 of SSR-4 [2].

2.26. In accordance with para. 4.2 (d) of SSR-4 [2], the operating organization is required to arrange for audits of criticality safety measures. This should include the examination of arrangements for emergency response, for example, emergency communications, evacuation routes and signage. Checks should be performed by the criticality safety staff who performed the safety assessments to confirm that the data used, and the implementation of criticality safety measures, are correct. Audits should be performed by personnel who are independent of those that performed the safety assessments or conducted the criticality safety activities. The data from audits should be documented and submitted for management review and for action, if necessary.

**Resource management**

2.27. The operating organization is required to provide adequate resources (both human and financial)
for the safe operation of the facility or activity (see Requirement 9 of GSR Part 2 [5]), including resources for mitigating the consequences of criticality accidents. The management of the operating organization, in particular the person responsible for criticality safety, should participate in the following:

(a) Determining the necessary competence of criticality safety staff, and providing training, as necessary;

(b) Preparing and issuing specifications and procedures on criticality safety;

(c) Supporting and performing criticality safety assessment;

(d) Having frequent personal contact with personnel, including observing work in progress.

2.28. The responsibilities, knowledge and training for ensuring criticality safety should be clearly specified by the operating organisation. The individuals having these responsibilities should be formally appointed by the operating organisation. Criticality safety staff should be knowledgeable about the physics (both static and kinetic) of nuclear criticality and the associated national and international safety standards, codes and best practices, and should be familiar with the design and operation of relevant facilities and the conduct of relevant activities. The criticality safety staff should be independent of the operations management, to the extent necessary.

2.29. All activities that might affect criticality safety are required to be performed by suitably qualified and competent personnel: see para. 9.83 of SSR-4 [2]. The operating organization should ensure that these personnel receive training and refresher training at suitable intervals, appropriate to their level of responsibility. In particular, personnel involved in activities with fissile material should understand the nature of the hazard posed by fissile material and how the risks are controlled by the established safety measures, operational limits and conditions, and operating procedures. The criticality safety staff should provide assistance in the training of operating personnel, provide technical guidance and expertise for the development of operating procedures, and check and validate all operations that might need criticality control.

2.30. The management system for criticality safety is required to include procurement activities and should be extended to include suppliers: see para. 4.35 and Requirement 11 of GSR Part 2 [5]. The operating organization should ensure, through audits, that suppliers (e.g. designers and safety analysts) have management systems that adequately address criticality safety.

2.31. Any hardware and software based process items and equipment that are necessary for work to be performed in a safe manner should be identified, provided and maintained. Calculation tools (e.g. computer codes) that are used for criticality safety assessment should be identified and are required to be verified and validated in accordance with para. 6.145 of SSR-4 [2]. Equipment and items that are used for criticality safety monitoring, data collection, verifications and tests should be qualified for the operating environmental conditions and should be calibrated, as necessary.
Process implementation

2.32. All operations to which criticality safety is pertinent are required to be performed in accordance with approved procedures and instructions that specify all the parameters that they are intended to control and the criteria to be fulfilled: see para. 9.83 of SSR-4 [2]. The operating procedures should cover operational states and credible abnormal conditions.

2.10. To facilitate the implementation of operating procedures used to ensure subcriticality, management should ensure that operating personnel involved in the handling of fissile material are also involved in the development of the operating procedures.

- Management should clearly specify which personnel have responsibilities. The assessments for ensuring modifications to facilities or activities, or proposals for introduction of new activities, are required to consider the implications for criticality safety.

- Management should ensure that suitably qualified: see paras 6.141 and experienced staff for criticality 9.83 of SSR-4 [2]. The safety are provided.

- Management should ensure that any modifications to existing facilities or activities, or introduction of new activities undergo assessments of modifications affecting fissile material that have a safety significance should be notified to the regulatory body to allow review and assessment and approval at the appropriate level before they the modifications are implemented, and should also ensure that modifications having major safety significance are required to be subjected to procedures for design, construction and commissioning that are equivalent to those applied to the whole facility or activity: see para. 9.59 of SSR-4 [2]. The facility or activity documentation is required to be updated to reflect modifications, and the operating personnel, including supervisors, are retrained, as appropriate, prior to the implementation of the modifications.

- Management should ensure that operating personnel receive training and refresher training at suitable intervals, appropriate to their fissile material safety measures and operational limits and conditions.

- Management should arrange for internal and independent inspections of the criticality safety measures, including the examination of arrangements for emergency response, for example, emergency evacuation routes and signage. Independent inspections should be documented and submitted for management review and for action, if necessary.

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*These inspections are in addition to the inspections performed by the regulatory body.*
Management should ensure that criticality safety assessments and analyses are conducted, documented and periodically reviewed.

2.11-2.34. Management should ensure that adequate resources will be available to mitigate training on the consequences modifications: see Requirement 61 of an accident SSR-4 [2].

1.7 Management should ensure that an effective safety culture is established in the organization [1].

Management should ensure that regulatory requirements are complied with.

2.12-2.35. The nature of the criticality hazard is such that deviations towards insufficient subcritical margins may not be immediately obvious; that is, there may be no obvious indication that the effective neutron multiplication factor is increasing. If unexpected operational deviations occur that are not foreseen in the criticality safety assessment, operating personnel should immediately consult the criticality safety staff for advice on how to place the system into a known safe condition. Operating personnel handling fissile material should therefore inform their supervisor in the event of any unforeseen operational deviations.

2.36. Throughout the lifetime of the facility or the duration of an activity, operations to which criticality safety is pertinent involve different groups and interfaces with other areas, such as those related to nuclear security and to the system of accounting for and control of nuclear material: see Requirement 75 of SSR-4 [2]. The operations with such interfaces should be identified, coordinated, planned, and conducted to ensure effective communication and clear assignment of responsibilities. Communications regarding safety and security should ensure that confidentiality of information is maintained. This includes the system of accounting for, and control of, nuclear material, for which information security should be coordinated in a manner ensuring that subcriticality is not compromised.

Measurement, assessment, evaluation and improvement

2.13-2.37. Audits performed by the operating organization of facilities and activities (see para. 2.26), as well as proper control of modifications to facilities and activities (see para. 2.34) are particularly important for ensuring subcriticality should be carried out regularly and the results should be evaluated by the operating organization and corrective actions taken if necessary. There is also a danger that conditions may change slowly over time in response to factors such as ageing of the facility or owing to increased production pressures: see para. 4.2 (d) of SSR-4 [2].

2.14-2.38. Most criticality accidents in the past and near-miss events have had multiple causes, often. In many cases, initiating events could have been identified by operating personnel and supervisors, and unsafe conditions corrected before the criticality accident occurred. This highlights the importance of sharing operating experience, (i.e. without breaching any arrangements for information security), of training operating personnel and of independent inspections. These activities should be part of the
management system audits.

2.15. Deviation from operational procedures and unforeseen changes in operations or in operating conditions are required to be reported and promptly investigated by the operating organization: see paras 9.34, 9.35 and 9.84 of SSR-4 [2]). The investigation should be carried out to analyse the causes of the deviation, to identify lessons to be learned, and to determine and implement corrective actions to prevent a recurrence. In accordance with the graded approach, the depth and extent of the investigation should be proportionate to the safety significance of the event. It should include an analysis of the operation of the facility and of or conduct of the activity including human factors, and a review of the criticality safety assessment and analyses that were previously performed, including the safety measures that were originally established.

2.16. Useful information on the causes and consequences of previous criticality accidents and the lessons learned is provided in Ref. [17].

2.17. The management system include a means of incorporating lessons learned from SSR-4 [2] states that “the operating experience and accidents organisation shall establish a programme to learn from events at the facility and events at other nuclear fuel cycle facilities in the State and in other States, to improvement in operational practices and assessment methodology for establishing a system for the feedback of and in the nuclear industry worldwide.” Recommendations on operating experience programmes are provided in SSG-50 [16] (see also para. 2.7).
3. MEASURES FOR ENSURING CRITICALITY SAFETY

GENERAL

THE MEASURES THAT SHOULD BE TAKEN

GENERAL PRINCIPLES FOR ENSURING CRITICALITY SAFETY

3.1. Consideration of criticality safety should be used to determine the following:

(a) The design and arrangement of engineered safety measures;
(b) The need for instrumentation for ensuring that the operational limits and conditions are adequately monitored and controlled;
(c) The need for additional administrative measures for ensuring that the operational limits and conditions are adequately controlled.

3.2. When determining the measures for ensuring the criticality safety of systems in which fissile material is handled, processed, used or stored, it is required to be considered: see para. 6.141 of SSR-4 [2]. Two vital parts of this concept are passive safety features and fault tolerance. For criticality safety (i.e., the design should be such that a failure occurring anywhere within the systems provided to fulfil each safety function will not cause the system to achieve criticality).

3.3. With regard to fault tolerance, para. 6.142 of SSR-4 [2] states:

“For the prevention of criticality by means of design, the double contingency principle shall be the preferred means of ensuring fault tolerance [1]. Approach. For application of the double contingency principle, the design for a process shall include sufficient safety factors to require at least two unlikely, independent and concurrent changes in process conditions before a criticality accident is possible.”

Defence in depth

3.4. The facility or activity should be designed and operated or conducted so that it provides defence in depth against credible abnormal conditions and accidents: see Requirement 10 of SSR-4 [2]. This is achieved by the provision of different levels of protection with the objective of preventing failures, or, if prevention fails, ensuring detection and response.

*To ensure safety, the design should be such that a failure occurring anywhere within the safety systems provided to carry out each safety function will not cause the system to achieve criticality.*
mitigating the consequences to ensure that the failure is detected and compensated for or corrected. The primary objective should be to adopt safety measures that prevent a criticality accident. However, in line with the principle of defence in depth, safety measures should also be put in place required to mitigate the consequences of such an accident. See para. 6.19 of SSR-4 [2].

3.2.3.5. An overview of the levels of defence in depth (see para. 2.12 of SSR-4 [2]) in relation to criticality safety is provided in Table 1. In applying the concept of defence in depth as described in, the fourth level of defence in depth, which deals with ensuring the confinement function to limit radioactive releases, might not be fully applicable in the context of criticality safety. However, for mitigation of the radiological consequences of a criticality accident, the fifth level of defence in depth has to be applied, with consideration given to the requirements for emergency preparedness and response established in GSR Part 7 [9] (see also Section 6 of this Safety Guide).

3.1. Application of the concept of defence in depth ensures that, if a failure occurs, it will be detected and compensated for, or corrected by appropriate measures. The objective for each level of protection is described in Ref. [1], on which the following overview of defence in depth is based.

**TABLE 1. OVERVIEW OF LEVELS OF DEFENCE IN DEPTH IN RELATION TO CRITICALITY SAFETY**

<table>
<thead>
<tr>
<th>Level</th>
<th>Objective</th>
<th>Means of protection</th>
</tr>
</thead>
<tbody>
<tr>
<td>Level 1</td>
<td>Prevention of deviations from normal operation and prevention of system failures of systems important to safety.</td>
<td>Conservative Incorporation of the double contingency principle in design, construction, maintenance (see para. 3.3); and operation in accordance the assurance of subcriticality under normal and all credible abnormal conditions, with an appropriate margin of subcriticality for safety margins, engineering practices and quality levels.</td>
</tr>
<tr>
<td>Level 2</td>
<td>Detection and interception control of deviations from normal operation in order to prevent anticipated operational occurrences credible abnormal conditions from escalating to</td>
<td>Control, indication and alarm systems; operating procedures to maintain the</td>
</tr>
<tr>
<td>Level</td>
<td>Objective</td>
<td>Means of protection</td>
</tr>
<tr>
<td>-------</td>
<td>-----------</td>
<td>---------------------</td>
</tr>
<tr>
<td>Level 2</td>
<td></td>
<td>facility within operational states. In the event that an unlikely change in process conditions occurs, administrative or engineered (or combinations thereof) features to detect and correct the change in process conditions in order to limit the likelihood of a second change in process conditions occurring concurrently.</td>
</tr>
<tr>
<td>Level 3</td>
<td>Control of the events within the design basis (or the equivalent) to prevent a criticality accident.</td>
<td>Safety measures, and multiple and as far as practicable independent barriers and procedures for the control of events called for controlling accidents cannot be directly transposed to a criticality accident.</td>
</tr>
<tr>
<td>Level 4</td>
<td>Mitigation of the consequences of accidents in which the design basis (or the equivalent) of the system may be exceeded and ensuring that the radiological consequences of a criticality accident are kept as low as practicable.</td>
<td>Provision of criticality detection and alarm systems and procedures for safe evacuation and accident management. Measures designed to terminate the criticality accident, e.g. injection of neutron absorbers. Use of shielding and calculated dose contours to minimize exposure.</td>
</tr>
<tr>
<td>Level 5</td>
<td>Mitigation of radiological consequences of release of</td>
<td>Provision of an emergency plan.</td>
</tr>
<tr>
<td>Level</td>
<td>Objective</td>
<td>Means of protection</td>
</tr>
<tr>
<td>-------</td>
<td>-----------</td>
<td>---------------------</td>
</tr>
<tr>
<td></td>
<td>radioactive material release</td>
<td>control centre and plans for on-site and off-site emergency response</td>
</tr>
</tbody>
</table>

**Passive safety**

3.3.6. The passive safety of the facility or activity should be such that the system will remain subcritical without the need for active engineered safety measures or administrative safety measures (i.e. other than verification that the properties of the fissile material and changes in reflection, absorption and moderation are covered by the design). For example, the facility or activity could be designed using the assumption that fissile material is always restricted to equipment with a favourable geometry. Special care is then necessary to avoid unintentional transfer to an unfavourable geometry.

**Fault tolerance**

3.4.7. The design should take into account fault tolerance in order to replace or complement passive safety measures (if any). The double contingency principle (see para. 3.3) is required to be the preferred means of ensuring fault tolerance by design. By virtue of applying this principle, a criticality accident cannot occur unless at least two unlikely, independent and concurrent changes in process conditions have occurred, (see also Requirement 23 of SSR-4).

1.8. According to the double contingency principle, if a criticality accident could occur owing to the concurrent occurrence of two changes in process conditions, it should be shown that:

- The two changes are independent (i.e. not caused by a common cause failure);
- The probability of occurrence of each change is sufficiently low.

3.6.9. The system’s characteristics of a system should meet the recommendations in para. 2.112, in order that each change in process conditions can be detected (e.g. monitored) by suitable and reliable means within a timeframe that allows the necessary countermeasure to be taken.

3.7.10. The system design should follow the fail-safe principle and, such that a component failure

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10 A system with a favourable geometry is one whose dimensions and shape are such that a criticality event cannot occur even with all other parameters at their worst credible conditions configuration.
will not result in a criticality accident. In meeting Requirement 23 of SSR-4 [2], the safety measures should fulfill the single failure criterion, i.e. be designed to ensure that no single failure or event, such as a component failure, a function control failure or a human error (e.g. an instruction not followed), can result in a criticality accident (the single failure criterion).

3.8.3.11. Where failures or maloperations incorrect operation of the system or perturbations or malfunctions in the system could lead to an unsafe condition, the characteristics of the system should be such that key parameters only deviate from their normal operating values at a rate such that detection, intervention and recovery can be carried out properly in order performed sufficiently well to prevent a criticality accident. Where this is not possible, it should be ensured that sufficient and appropriate additional safety measures are provided to prevent (with a high degree of confidence) the initiating event from developing into a criticality accident.

SAFETY FUNCTIONS AND MEASURES

SAFETY FUNCTIONS AND SAFETY MEASURES FOR CRITICALITY SAFETY

3.9.3.12. The safety functions needed for ensuring subcriticality should be determined and the safety measures for fulfilling these functions should be defined; (see also para. 6.139 of SSR-4 [2]). The definition and substantiation of the safety functions should be based determined on the basis of an analysis of all initiating or aggravating events and their combinations relevant to criticality safety arising from credible abnormal conditions, including human error, internal and external hazards, and loss or failure of structures, systems and components important to safety in operational states and in design basis accidents (or the equivalent).

3.10.3.13. In accordance with para. 6.68 of SSR-4 [2], and applying the lessons from criticality accidents, the selection of preventive safety measures put in place should observe the following hierarchy:

(1) Inherent safety of the process;

(2) Passive engineered safety measures that do not rely on control systems, active engineered safety measures or human intervention;

(3) Automatically initiated active engineered safety measures (e.g. an automatically initiated shutdown or process control system);

(4) Administrative safety measures:

(i) Active engineered safety measures initiated manually by operating personnel (e.g. operating personnel initiating a shutdown system in response to an indicator or alarm);

(ii) Safety measures provided by operating personnel (e.g. operating personnel a shutdown valve...
in response to a mass limit that is implemented by an indicator or alarm, or operator weighing a container and verifying that the system mass limit will not be exceeded prior to introducing the container into normal operational limits by adjusting controls (a glovebox).

3.14. The hierarchy of safety measures in para. 3.13 gives preference to inherently safe design and passive safety. If subcriticality cannot be ensured through these means, further safety measures should be employed to minimize the probability of a criticality accident and to mitigate the consequences of such an accident on workers, the public and the environment. This does not mean that the application of any safety measure towards the top of the hierarchy precludes the provision of other safety measures where they can contribute to defence in depth.

3.14-3.15. In addition to the hierarchy of preventive safety measures in para. 3.13, and consistent with the concept of defence in depth, mitigatory safety measures (e.g. shielding, criticality incident detection systems and emergency response) should are required to be employed to the extent practicable, in accordance with paras 6.149–6.151 of SSR-4 [2].

3.2. Safety should be ensured by means of design features and characteristics of the system that are as near as possible to the top of the list provided in para. 3.12, but this should not be interpreted to mean that the application of any safety measure towards the top of the list precludes the provision of other safety measures where they can contribute to defence in depth.

3.3. The hierarchy of safety measures gives preference to passive safety. If subcriticality cannot be ensured through this means, further safety measures should be employed.

3.12-3.16. The safety measures put in place that are applied should be related to the control of one or more parameters and their combinations. Examples of the control parameters are given in para. 3.17.

Control parameters for criticality safety

3.17. The subcriticality of system can be demonstrated by calculating \( k_{\text{eff}} \) and/or controlled by limiting Paragraph 6.143 of SSR-4 [2] states:

“Criticality safety shall be achieved by keeping one or more of the following parameters of the system within subcritical limits…:

— Mass and enrichment of fissile material present in a process;
— Geometry (limitation of the dimensions or shape) of processing equipment;
— Concentration of fissile material in solutions;
— Degree of moderation;
— Control of reflectors;
— Presence of appropriate neutron absorbers.”
The control parameters that should be considered for ensuring subcriticality include (but are not limited to) the following:

(a) **Restriction** on the dimensions or shape of the system to ensure a favourable geometry.

(b) **Limitation** on the mass of fissile material within a system to a subcritical mass. For example, in order to apply the subcritical mass limit may be specified to be less than half the minimum critical mass (incorporating a suitable safety factor) so that inadvertent ‘over-batching’ of fissile material does not lead to criticality. Consideration may also need to be given to the potential for multiple over-batching of fissile material, as a credible abnormal condition: see para. 9.85(a) of SSR-4 [2].

(c) **Limitation** on the concentration of fissile nuclides, for example within a homogeneous hydrogenated mixture or within a solid.

(d) **Limitation** on the type and quantity of neutron moderating material associated with the fissile material.

(e) **Limitation** on the isotopic composition of the elements in the fissile material present in the system.

(f) **Limitation** on the density of the fissile material.

(g) **Limitation** on the amount, geometrical distribution and form of neutron reflecting material surrounding the fissile material.

(h) Ensuring the presence, geometrical distribution and integrity of neutron absorbers in the system or between separate systems that are individually subcritical.

(i) **Limitation** on the minimum separation distance between separate systems that are individually subcritical.

The control parameter limitations set out limits in para. 3.18 can be evaluated either by multiplying the critical parameter value determined for the system’s particular conditions by a safety factor, or by calculating the value of the parameter value that meets the criterion that \(k_{\text{eff}}\) is system to be subcritical with a sufficient margin. In deriving safety margins, consideration should be given to the degree of uncertainty in a system’s conditions, the probability and rate of change in those conditions, the uncertainties in calculations, if used, and the consequences of a criticality accident. As stated in para. 6.140 of SSR-4 [2], “[c]riticality evaluations and calculations shall be performed on the basis of conservative assumptions.”

**Factors affecting subcriticality**

In many cases, limits on the nuclide composition of the elements in the fissile material...
material, or restrictions to a certain type and chemical compound of the fissile material, or a combination of both, are essential for ensuring criticality safety in many cases. Effective safety measures should be applied to ensure that:

(a) The limits on the nuclide composition of the elements in the fissile material are complied with;

(b) The compound (chemical and physical form) to be used cannot change to become a more reactive compound;

(c) A mixture of different types or different compounds resulting in a higher effective neutron multiplication factor cannot occur.

The events described in (b) and (c) could occur in specific situations, for example, (e.g., the precipitation of a U/Pu nitrate solution or modification of the diameter of pellets), and both such events should be taken into account in the criticality safety assessment and proven to be subcritical.

3.16.3.21. The presence of neutron moderating materials should be considered, as these can significantly reduce the critical mass of the fissile material. Hydrogen and carbon contained in materials such as water, oil, graphite and polyethylene are common moderators. Low atomic mass, low neutron absorption materials (such as deuterium, beryllium and beryllium oxide) are less common but can be very effective moderators. Consideration should be given to the replacement of a moderator and/or reflector with an alternative substance that has more favourable properties; for example, there is the possibility that hydrocarbon-based oils could be replaced with oils containing (for instance) fluorine or chlorine.

3.17.3.22. The presence of neutron reflecting material should be considered. Material present outside the system of fissile material will act as a neutron reflector and can increase the effective neutron multiplication factor of the system. Criticality safety assessments usually consider a light water reflector (full density water) with a thickness sufficient to achieve the maximum effective neutron multiplication factor, known as ‘total reflection’ or ‘full light water reflection’. However, the possible presence of other reflector materials (such as polyethylene, concrete, steel, lead, beryllium and aluminium), or several reflector materials used in combination, should be considered, if this could result in a greater increase in the effective neutron multiplication factor than by full light water reflection.

3.18.3.23. The presence of neutron absorbers should be considered. Neutron absorbers are mainly effective for thermal neutron systems. Therefore, any neutron spectrum hardening, i.e. an increase in the distribution of higher energy neutrons, caused by operating conditions or credible abnormal conditions, should be considered, as this may result in a decrease in the effectiveness of the neutron absorption. Therefore, when the safety function of a neutron absorber is necessary, being considered, appropriate safety measures should be applied to ensure that the effectiveness of the neutron absorber...
remains sufficient. Consideration should also be given to monitoring the credible long term degeneration and/or-degradation of neutron absorbers and/or situations that could cause such degradation.

3.19-3.24. The geometrical distribution of neutron absorbers and credible changes in their distribution should be considered. Changes in the geometrical distribution of neutron absorbers could include slumping, evaporation and compression.

3.20-3.25. Neutron absorbers that are homogeneously distributed in a thermal neutron system are usually more effective than if they were heterogeneously distributed (however, heterogeneously distributed absorbers may be easier to control by administrative means). In a thermal neutron system consisting of a heterogeneous arrangement of fissile material and a fixed neutron absorber (e.g. the storage of fuel assemblies), the neutron absorber may be more effective the closer it is located to the fissile material. Any material (e.g. water, steel) located between the absorber and the fissile material can change the effectiveness of the absorber. Solid, fixed neutron absorbers should be tested and/or validated prior to first use in order to demonstrate the presence and uniformity of the distribution of the absorber isotope (e.g. $^{10}$B). Demonstration of the continued presence and effectiveness of neutron absorbers throughout their operational lifetime should be considered.

3.21-3.26. Material (e.g. steam, water mist, polyethylene, concrete) located between or around fissile material may act not only as a reflector but also as a moderator and/or a neutron absorber and can therefore increase or decrease the effective neutron multiplication factor of the system. Any change in the effective neutron multiplication factor will be dependent on the type and density of the material positioned between or around the fissile material. Materials containing hydrogen and materials with low density (such as steam or foam) can cause a significant change in the effective neutron multiplication factor. The inclusion or omission of any materials from the criticality safety assessment should be justified by evaluating the effect of their treatment on the effective neutron multiplication factor.

3.22-3.27. Neutron interaction between units of equipment containing fissile material should be considered, as this interaction can affect the effective neutron multiplication factor of the system. This control parameter can be used to ensure criticality safety, for example by specifying minimum separation distances (or in some cases maximum distances, e.g. to limit interstitial moderation between units of fissile material) or by introducing screens of neutron absorbers. Wherever practicable, separation should be ensured by engineered means, for example fixed storage racks for storage of arrays of drums containing fissile material.

3.23-3.28. Heterogeneity. The heterogeneity of materials such as swarf (turnings, chips or metal filings) or fuel pellets can result in effective neutron multiplication factors greater than those calculated by assuming the factor for a homogeneous mixture, particularly for low enriched uranium systems or for mixed uranium and plutonium. Therefore, the degree of heterogeneity or homogeneity used or assumed in the criticality safety assessment should be justified. Safety measures should be applied that ensure that
the heterogeneity of the fissile material could not result in a higher effective neutron multiplication factor than that considered.

3.24, 3.29. The temperature of materials might cause changes in density and in neutron cross-section, which might affect the effective neutron multiplication factor. This should be considered in the criticality safety assessment.

ENGINEERED SAFETY MEASURES

PASSIVE ENGINEERED SAFETY MEASURES FOR CRITICALITY SAFETY

Passive engineered safety measures use passive components to ensure subcriticality. Such measures are highly preferred because they provide high reliability, cover a broad range of criticality accident scenarios, and little operational support to maintain their effectiveness as long as ageing aspects are adequately managed. Human intervention is not necessary. Advantage may be taken of natural forces, such as gravity, rather than relying on electrical, mechanical or hydraulic action. Passive engineered safety measures for criticality safety

3.25, 3.30. Passive engineered safety measures are highly preferred. Like active components, passive components are subject to (random) degradation and to human error during installation and maintenance activities. They require Passive components should be subject to surveillance or periodic verification and, as necessary, maintenance. Care should be taken that boundary conditions, necessary for the effectiveness of the passive measure, will be maintained. Examples of passive components are geometrically favourable pipes, vessels and structures, solid neutron absorbing materials, and the form of fissile material. When considering the reliability of these types of component, administrative failure modes should be taken into account.

3.26, 3.31. Certain components that function with very high reliability based on the basis of irreversible action or change may be designated as passive components.

3.27, 3.32. Certain components, such as rupture discs, check valves, safety valves and injectors, have characteristics that required special consideration before designation as an active or passive

11 Passive engineered safety measures use passive components to ensure subcriticality, which might take advantage of natural forces, such as gravity, rather than relying on electrical, mechanical or hydraulic action. Such measures are highly preferred because human intervention is not necessary, the measures provide high reliability, cover a broad range of criticality accident scenarios, and need little operational support to maintain their effectiveness provided that ageing aspects are adequately managed.
component. Any engineered component that is not a passive component is designated as an active component, although it may be part of either an active engineered safety measure or an administrative safety measure.

**Active engineered safety measures for criticality safety**

3.33. Active engineered safety measures use active components such as electrical, mechanical or hydraulic hardware\(^{12}\) should be used in addition to ensure subcriticality. Active components act by a process variable important to criticality safety (or by being actuated through the instrumentation and control system) and providing automatic action to place the system in a safe condition, without the need for human intervention. Active engineered passive safety measures should be used when and where passive engineered safety measures are not feasible. However, active Active components are subject to random failure and degradation and to human error during operation and maintenance activities. Therefore, components of high quality and with low failure rates should be selected in all cases. Fail-safe designs should be employed, if possible, and failures should be easily and quickly detectable. Redundant systems and components should be common cause failure. Active engineered components require

3.34. Paragraph 6.92 of SSR-4 [2] states:

“The principles of redundancy and independence shall be applied as important design principles for improving the reliability of functions important to safety. Depending on their safety classification, items important to safety shall be physically separated and the use of shared systems shall be minimized.”

In addition, para. 6.141 of SSR-4 [2] states that “[s]afety controls for criticality shall be independent, diverse and robust.” Active engineered components are required to be subject to surveillance, periodic testing for functionality, and preventive and corrective maintenance to maintain their effectiveness; see Requirements 26 and 65 of SSR-4 [2].

3.35. Examples of active components are neutron or gamma monitors, (see paras 6.32–6.56), computer controlled systems for the movement of fissile material, trips based on process parameters (e.g. conductivity, flow rate, pressure and temperature), pumps, valves, fans, relays and transistors. Active components with actions that require necessitate a human action in response to an engineered stimulus (e.g. the response to an alarm or to a value on a weighing scale) should be considered as administrative safety measures, although they contain active engineered components (see paras 3.35–3.47). When

\(^{12}\) Active engineered safety measures use active components such as electrical, mechanical or hydraulic hardware to ensure subcriticality. Active components act by responding to a process variable that is important to criticality safety (or by being actuated through the instrumentation and control system) and providing automatic action to place the system in a safe condition, without the need for human intervention.
considering the reliability of these types of component, administrative failure modes should be taken into account.

ADMINISTRATIVE SAFETY MEASURES

ADMINISTRATIVE SAFETY MEASURES FOR CRITICALITY SAFETY

General considerations for administrative safety measures for criticality safety

3.29.3.36. When administrative safety measures are employed, particularly procedural controls, it should be demonstrated in the criticality safety assessment that credible deviations from such measures have been exhaustively studied and that combinations of deviations that could lead to a dangerous situation criticality accident are understood. Specialists in human performance and human factors should be consulted to develop the procedural controls, to inform management as to assess the robustness, or otherwise, of the procedural controls, and to seek identify improvements, where appropriate.

3.30.3.37. The use of administrative safety measures should be incorporated into the management system of the operating organization (see para. 2.1), and the use of such measures should include, but are not limited to, consideration of the following and should be incorporated into the comprehensive criticality safety programme (see para. 2.1):

(a) Specification and control of the nuclide composition of the elements in the fissile material, the fissile nuclide content, the mass, density, concentration, chemical composition and degree of moderation of the fissile material, and the spacing between systems of fissile material.

(b) Determination and demarcation of criticality controlled areas (i.e. areas authorized to contain significant quantities of fissile material) and specification of the control parameters associated with such areas: specification specification (and, where applicable, labelling for of materials (e.g. fissile material, or neutron moderating materials, neutron absorbing or reflecting materials); and specification specification (and, where applicable, labelling for the of control parameters and their associated limits on which subcriticality depends. A criticality controlled area is should be defined by both the characteristics of the fissile material within it and the control parameters used.

(c) Control of access to criticality controlled areas where fissile material is handled, processed or stored.

(d) Separation between criticality controlled areas, and separation of materials within criticality controlled areas.

(e) Movement and control of materials within and between criticality controlled areas (including those
areas containing different fissile materials and/or with different control parameters), and spacing between moved and stored materials, (see also para. 6.147 of SSR-4 [2]).

(f) Procedural controls for record keeping systems (e.g. accounting for fissile material).

- Movement and control of fissile material between criticality controlled areas containing different fissile materials and/or with different control parameters.

(g) Movement and control of materials from areas without criticality safety control (e.g. wastewater processing areas) to criticality controlled areas or vice versa (e.g. flow of effluent waste streams from controlled to uncontrolled processes) (see also Requirement 28 of SSR-4 [2]).

(h) Use of neutron absorbers, and control of their continued presence, distribution and effectiveness.

(i) Procedures for use and control of ancillary systems and equipment (e.g. vacuum cleaners in criticality controlled areas and control of filter systems in waste air and off-gas systems).

(j) Quality assurance management, periodic inspection (e.g. control of continued favourable geometries), maintenance, and the collection and analysis of operating experience.

(k) Procedures for use in the event of credible abnormal conditions (e.g. deviations from operating procedures, credible alterations in process or system conditions).

(l) Procedures for preventing, detecting, stopping and containing leakages, and for removing leaked materials.

(m) Procedures for firefighting (e.g. the use of hydrogen-free or very low hydrogen content fire extinguishing materials).

(n) Procedures for the control and analysis of design modifications and of changes in operating procedures.

(o) Procedures for criticality safety assessment and analysis.

(p) Procedures for the appointment of suitably qualified and experienced staff for criticality safety staff.

(q) Procedures for training to operating personnel and criticality safety staff.

(r) Ensuring that the procedures are understood by operating personnel and contractors working at the facility.

(s) Control of the facility configuration.

(t) The safety functions and safety classification of the structures, systems and components important to safety (for example, this is applicable e.g. in relation to the design, procurement, administrative oversight of operations, and to maintenance, inspection, testing and examination).
Operating procedures

3.38. Operating procedures are required by Requirement 63 of SSR-4 [2], and approved procedures in relation to criticality safety are required by para. 9.83 of SSR-4 [2]. These procedures should be written with sufficient detail for a qualified individual to be able to perform the activities without the need for direct supervision. The aims of operating procedures should be as follows:

(a) To facilitate the safe and efficient conduct of operations;
(b) To include those controls, limits and measures that are important for ensuring subcriticality;
(c) To include mandatory operations, advice and guidance for credible abnormal conditions and accident conditions;
(d) To include appropriate links between procedures in order to avoid omissions and duplications and, where necessary, to clearly specify the conditions of entry to and exit from other procedures;
(e) To be simple and readily understandable to operating personnel.

3.39. Procedures should be reviewed in accordance with the management system. Such reviews should incorporate any changes and lessons from feedback of operating experience, and should be supported by periodic training. As appropriate, this should include review by supervisors and the relevant criticality safety staff. Any changes to operating procedures should be subject to approval by managers responsible for ensuring subcriticality.

Responsibilities and authorities for criticality safety

3.40. The operating organization has the responsibility for overseeing the implementation of the criticality safety measures and for implementing an appropriate quality management programme. The relevant authorities and responsibilities are required to be documented in the management system (see paras. 2.22 and 2.23).

3.41. The operating organization may delegate authority for the implementation of specific criticality safety measures to supervisors. The authority that is permitted to be delegated to a supervisor should be specified and documented in the management system. The primary responsibility for safety remains with the operating organization: see Requirement 2 of SSR-4 [2].

3.42. Authority for the implementation of the quality management programme should be assigned to persons who are independent of the operating personnel.

3.43. Requirement 12 of GSR Part 2 [5] states that “[i]ndividuals in the organization, from senior managers downwards, shall foster a strong safety culture.” This should ensure that all personnel understand the importance of ensuring subcriticality and the necessity of adequately implementing the
criticality safety measures. For this purpose, the operating organization should provide the following:

(a) Criticality safety staff who are independent of operating personnel, and who report (along with other safety experts) to a manager with responsibility for safety at the highest level of the organization;

(b) The organizational means for ensuring that the criticality safety staff provide managers, supervisors and operating personnel with periodic training on criticality safety, to improve their safety awareness and behaviour (see para. 9.83 of SSR-4 [2]);

(c) The organizational means for ensuring that criticality safety staff are provided with periodic training on criticality safety that is suited to their roles, responsibilities and operations;

(d) The organizational means for ensuring that periodic reviews of criticality safety assessments (see Section 4) are undertaken;

(e) The organizational means for ensuring that the criticality safety programme and its effectiveness are continually reviewed and improved.

3.44. Records of participation in criticality safety training should be maintained and used to ensure that routine refresher training is provided.

3.45. The criticality safety staff should be responsible for the following:

(a) Performing and documenting criticality safety assessments for systems of, or areas with, fissile material;

(b) Ensuring the accuracy of the criticality safety assessment, by, whenever possible, directly observing the activity, processes or equipment, as appropriate, and encouraging operating personnel to provide feedback on operating experience;

(c) Providing documented guidance on criticality safety for the design of systems of fissile material and for processes, and for the development of operating procedures;

(d) Specifying the operational limits and conditions for ensuring criticality safety;

(e) Specifying the necessary criticality safety measures and supporting their implementation;

(f) Determining the location and extent of criticality controlled areas;

(g) Assisting in determining the location of criticality detection and alarm systems and development of the associated emergency arrangements, and conduct of periodic reviews of these arrangements;

(h) Assisting and consulting operating personnel, supervisors and management and maintaining contact with them to ensure familiarity with all activities involving fissile material;

(i) Conducting regular walkdowns of the facility and inspections of the activities;
(j) Assisting in the establishment, modification and review of operating procedures;
(k) Verifying and documenting criticality safety in relation to modifications or changes in the design of systems or in processes;
(l) Ensuring that training in criticality safety is provided periodically for operating personnel, supervisors and management.

3.46. Supervisors should be responsible for the following:
(a) Maintaining an awareness of the control parameters and associated limits for criticality safety relevant to systems for which they are responsible;
(b) Monitoring and documenting compliance with the limits of the control parameters;
(c) Ensuring that inspection, testing and maintenance programmes for engineered safety systems are implemented;
(d) If there is a potential for unsafe conditions to occur due to a deviation from normal operations, stopping the work in a safe way and reporting the event, as necessary;
(e) Promoting a questioning attitude from personnel and demonstrating a strong safety culture including giving priority to safety over the needs of production.

3.47. In relation to criticality safety, the responsibilities of operating personnel and other personnel should include the following:
(a) To cooperate and comply with management instructions and procedures;
(b) To adopt and contribute to a questioning attitude and strong safety culture;
(c) If there is a potential for unsafe conditions to occur due to a deviation from normal operations, to stop work and report the event, as necessary.

IMPLEMENTATION AND RELIABILITY OF CRITICALITY SAFETY MEASURES

3.48. Implementation of a combination of different engineered and administrative safety measures is essential for the assurance of subcriticality: see para. 6.139 of SSR-4 [2]. In accordance with the principles of redundancy, diversity and independence (see Requirement 23 and para 6.141 of SSR-4 [2]) reliance can be placed on safety measures that have been already implemented in the facility or activity. Any such existing measures should be considered within the hierarchy of criticality safety measures described in paras 3.12–3.14.

3.49. Safety measures include quality management measures, inspection, testing and maintenance to ensure that the necessary safety functions are fulfilled and that criteria for reliability are met. Where administrative controls are necessary as part of a safety measure, these should be verified regularly.
3.50. Before the implementation of criticality safety measures, consideration should be given to a range of factors including the following:

(a) The complexity of implementing the safety measure;

(b) The potential for common cause failure of safety measures;

(c) The reliability claimed in the criticality safety assessment for the set of safety measures;

(d) The ability of operating personnel to recognize abnormality or failure of the safety measure;

(e) The ability of operating personnel to manage abnormal situations;

(f) The ageing management aspects;

(g) Feedback of operating experience.

3.51. Changes affecting criticality safety due to ageing of the facility should be considered. The ageing management programme is required to be coordinated with the criticality safety programme: see paras 9.53 and 9.83 of SSR-4 [2].

3.52. Ageing effects should be monitored and their potential impacts on criticality safety should be assessed. Where ageing has reduced criticality safety below acceptable levels, corrective measures are required to be implemented; see para. 4.2(d) of SSR-4 [2]. Changes that have been approved should be implemented in a timely manner. Periodic testing of items relied upon to ensure subcriticality should be performed to ensure that the criticality safety analysis remains valid for any actual or potential degradation in the condition of such items.

3.53. Before a new activity with fissile material is initiated, the level of criticality safety is required to be assessed (see para. 6.141 of SSR-4 [2]) and the necessary engineered and administrative safety measures should be determined, prepared and independently reviewed by personnel knowledgeable in criticality safety staff. Likewise, before an existing facility or activity is changed, the engineered and administrative safety measures should be revised and again independently reviewed and, as appropriate, revised. The introduction of a new activity may be subject to authorization by the regulatory body before it can be initiated.

**Operating procedures**
4. Procedures should be written with sufficient detail. **CRITICALITY SAFETY ASSESSMENT**

1.9 General considerations for a qualified individual to be able to perform the required activities without the need for direct supervision. Furthermore, operating procedures:

(a) Should facilitate the safe and efficient conduct of operations;

(b) Include those controls, limits and measures that are important for ensuring subcriticality;

(c) Mandatory operations, advice and guidance for anticipated operational occurrences and accident conditions;

(d) Should include appropriate links between procedures in order to avoid omissions and duplications, and, where necessary, should specify clearly conditions of entry to and exit from other procedures;

(e) Simple and readily understandable to operating personnel;

- Be periodically reviewed in conjunction with other facility documents, such as the emergency and the criticality safety assessment, to incorporate any changes and lessons learned from feedback of operating experience, and for training at predetermined intervals.

1.10 Procedures be reviewed in accordance with the management system. As appropriate, this review should include review by supervisors and the relevant staff for criticality safety and should be made subject to approval by managers responsible for ensuring subcriticality.

**Responsibility and delegation of authority**

1.11 The responsibility for overseeing the implementation of the criticality safety measures and for implementing appropriate quality assurance measures. Such authority and responsibility should be documented in the management system.

1.12 May delegate authority for the implementation of specific criticality safety measures to supervisors. The authority that is permitted to be delegated to a supervisor should be specified and documented in the management system.

1.13 Authority for the implementation of quality assurance measures and periodic inspections and the evaluation of the results of quality and periodic inspections should be assigned to persons who are independent of the operating personnel.

1.14 In and supervisors promote, in accordance with the requirements established in Ref. [3], a safety
culture all personnel aware of the importance of ensuring subcriticality and the necessity of adequately implementing the criticality safety measures. For this purpose, should provide the following:

(a) for criticality safety who are independent of operating personnel;

(b) The organizational means for ensuring that the relevant staff for criticality safety provide supervisors and operating personnel with periodic training on criticality safety, to improve their safety awareness and behaviour;

(c) The organizational means for ensuring that the relevant staff for criticality safety themselves are provided with periodic training on criticality safety;

(d) The organizational means for ensuring that periodic reviews of criticality safety assessments are undertaken;

(e) The organizational means for ensuring that the criticality safety programme and its effectiveness are continually reviewed and improved.

1.15—Records of participation in criticality safety training should be maintained and used to ensure that routine refresher training is appropriately recommended and instigated.

1.16—The relevant staff for criticality safety should be responsible for, at least, the following:

(a) Provision of documented criticality safety assessments for systems of, or areas with, fissile material;

(b) Ensuring the accuracy of the criticality safety assessment, by, whenever possible, directly observing the activity, processes or equipment, as appropriate, and encouraging operating personnel to provide feedback on operating experience;

(c) Provision of documented guidance on criticality safety for the design of systems of fissile material and for processes, and for the development of operating procedures;

(d) Specification of the criticality limits and conditions and required safety measures and support for their implementation;

(e) Determination of the location and extent of criticality controlled areas;

(f) Provision of assistance in determining the location of criticality detection and alarm systems and development of the associated emergency arrangements, and conduct of periodic reviews of these arrangements;

(g) Assisting and consulting operating personnel, supervisors and management and keeping close contact with them to ensure familiarity with all activities involving fissile material;

(h) Conducting regular walkdowns of the facility and inspections of the activities.
(i) Provision of assistance in the establishment and modification of operating procedures and review of these procedures;

(j) Documented verification of compliance with the criticality safety requirements for modifications or changes in the design of systems or in processes;

(k) Ensuring that training in criticality safety is provided periodically for operating personnel, supervisors and management.

1.17 Supervisors should be responsible for, at least, the following:

(a) Maintaining an awareness of the control parameters and associated limits relevant to systems for which they are responsible;

(b) Monitoring and documentation of compliance with the limits of the control parameters;

(c) If there is a potential for unsafe conditions to occur in the event of a deviation from normal operations, stopping work in a safe way and reporting the event as required;

(d) Promoting a questioning attitude from personnel and demonstrating safety culture.

1.18 In relation to criticality safety, the responsibilities of operating personnel and other personnel should be: to cooperate and comply with management instructions and procedures; to develop a questioning attitude and safety culture; and if unsafe conditions are possible in the event of a deviation from normal operations, to stop work and report the event as required.

IMPLEMENTATION AND RELIABILITY OF SAFETY MEASURES

1.19 Ensuring subcriticality in accordance with the concept of defence in depth usually requires the application of a combination of different engineered and administrative safety measures. Reliance be placed on safety measures already present in the facility or activity or applied to the system of interest. However, the hierarchy of criticality safety measures specified in para. 3. should be observed.

1.20 Consideration of criticality safety should be used to determine:

(a) The design and arrangement of engineered safety measures;

(b) The need for instrumentation for ensuring that the operational limits and conditions are adequately monitored and controlled;

(c) The need for additional administrative measures for ensuring that the operational limits and conditions are adequately controlled.

1.21 Safety measures should include a requirement for quality assurance measures, in-service inspection and testing, and maintenance to ensure that the safety functions are fulfilled and for reliability
are met. Where administrative controls are as part of a safety measure, these should be tested regularly.

1.22 Consideration should be given to other factors that could influence the selection of safety measures. These factors include, but are not limited to:

(a) The complexity of implementing the safety measure;
(b) The potential for common mode failure or common cause failure of safety measures;
(c) The reliability claimed in the criticality safety assessment for the set of safety measures;
(d) The ability of operating personnel to recognize abnormality or failure of the safety measure;
(e) The ability of operating personnel to manage abnormal situations;
(f) Feedback of operating experience.

Changes due to ageing of the facility should be considered. Ageing effects should be monitored and their impacts on criticality safety should be assessed. Periodic testing of items relied upon to ensure subcriticality should be performed to ensure that the criticality safety analysis remains valid for any actual or potential degradation in the condition of such items.
4.1 CRITICALITY SAFETY ASSESSMENT

GENERAL

4.1. Criticality safety assessments should use a deterministic approach, in which a set of conservative rules and requirements concerning facilities or activities involving fissile material is applied. In such an approach, the adequacy of safety measures in successfully minimizing, detecting and intercepting deviations in control parameters to prevent a criticality accident should be judged mainly against a set of favourable characteristics criteria, such as the independence, redundancy and diversity and independence of the safety measures, and whether the safety measures are engineered or administrative, or passive or active. Such considerations may also include a qualitative judgement of the likelihood of failure on demand for of these safety measures. If these rules and requirements are met, it is inferred that the criticality risk (see para. 4.2) is acceptably low. should be considered.

4.2. The scope and level of detail of the criticality safety assessment is required to reflect the type of practice and its operation and be consistent with the magnitude of the possible radiation risks arising from the facility or activity, in accordance with a graded approach: see Requirement 1 of GSR Part 4 (Rev. 1). [4].

4.2.4.3. It is also common to complement the deterministic approach to criticality safety assessment with a probabilistic approach. The probabilistic approach involves realistic assumptions regarding operating conditions and operating experience, rather than the conservative representation typically used in the deterministic approach. The probabilistic approach provides an estimate of the frequency of each initiating event that triggers a deviation from normal operating conditions and of the probabilities of failure on demand of any safety measures applied to minimize, detect or intercept the deviation. The frequency of the initiating event and the probabilities of failure of the safety measures can be combined to derive a value for the frequency of occurrence of criticality. By using this value and a measure of the consequences, an estimate of the criticality risk can be made and compared with risk targets or criteria, if any, for the facility or activity.

4.3.4.4. The probabilistic approach is used to evaluate the extent to which the safety of operations at the facility is well balanced and to provide additional insights into possible weaknesses in the design or

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13 Research facilities tend to have lower amounts of fissile material and flexible working procedures, and so human errors might be more prevalent. Fuel manufacturing facilities and fuel utilization facilities often have large amounts of fissile material and high production demands and use well defined processes, which depend on both human performance and the proper functioning of process equipment.
operation, which may can be helpful in identifying ways of further reducing the criticality risk. If the probabilistic assessment reveals an unusually high reliance of subcriticality protection on a single safety measure, strengthening or supplementing that measure should be considered. Difficulties in applying the probabilistic approach are sometimes encountered in criticality safety assessment if one or more of the safety measures includes the action of operating personnel as a significant component. The reliability of safety measures of this type can be very difficult to quantify. Also, in some cases there may might be a lack of data on the reliability for new types of equipment, hardware and/or software. Consideration should be given to the uncertainties in the calculated values of criticality risk derived by these methods when using the insights provided, especially if such values are to be used as a basis for significant modifications to a facility or activity.

PERFORMANCE OF A CRITICALITY SAFETY ASSESSMENT

4.4.4.5. In accordance with para. 6.138 of SSR-4 [2], a criticality safety assessment is required to be performed prior to the commencement of any new or modified activity involving fissile material. A criticality safety assessment should be carried out performed during the design, prior to stage, and also before and during construction, commissioning and operation of a facility or activity, and also prior to. A criticality safety assessment should also be performed before the on-site movement of fissile material, and before and during storage of fissile material and post-operational clean-out cleaning and decommissioning of the facility, transport and storage of fissile material.

4.5.4.6. The objectives of the criticality safety assessment should be to determine whether an adequate level of safety has been can be reasonably achieved, and to document the appropriate limits and conditions and safety measures required that are necessary to prevent a criticality accident. The criticality safety assessment should demonstrate and document the compliance of the design and procedures with appropriate safety criteria and safety requirements.

4.6.4.7. The criticality safety assessment should include a criticality safety analysis, which evaluates subcriticality for all operational states, i.e. for normal operation and anticipated operational occurrences and also during and after design basis accidents (or the equivalent) for credible abnormal conditions. The criticality safety analysis should be used to identify hazards, both internal and external, and to determine

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14 Requirements for criticality safety during the off-site transport of radioactive material are established in SSR-6 (Rev. 1) [3].

15 Specific transport requirements for criticality safety are included in the Transport Regulations [6].
the radiological consequences of a criticality accident.

4.7.4.8. All margins adopted in setting subcritical limits (see paras 2.8–2.12) should be justified and documented and there should be sufficient detail and clarity to allow an independent review of the judgements made and the chosen margins. When appropriate, this justification should be substantiated supported by reference to national regulations, to national and international standards or codes of practice, or to guidance notes that are compliant with these regulations and standards.

4.1. The criticality safety assessment and criticality safety analysis should be carried out by suitably qualified and experienced staff for criticality safety who are knowledgeable in all relevant aspects of criticality safety and are familiar with the facility or activity concerned, and should also include input from operating personnel.

4.8.4.9. In the criticality safety assessment, consideration should be given to the possibility of inappropriate (and unexpected) responses by actions by operating personnel in response to abnormal conditions. For example, the potential for operating personnel to respond to leaks of fissile solutions by catching the material in geometrically unfavourable equipment should be considered.

4.9.4.10. A systematic approach to the criticality safety assessment should be adopted, for example as outlined below, including, but not limited to, by the following steps:

(1) Definition of the reference fissile material, its constituents, chemical and physical forms, nuclear and chemical properties, etc.

(2) Definition of the processes and operations involving the fissile material.

(3) Methodology for conducting the criticality safety assessment.

(a) Verification and validation of the calculation methods, nuclear data;

(4) Performance of demonstrating the subcriticality of the design and procedures for operational states and credible abnormal conditions, including application of the double contingency principle and defence in depth, as appropriate. Identifying which criticality parameters are being controlled and their associated limits.

(5) Verifying and validating the calculation methods, including the computer codes, nuclear data and the procedures for using these methods, codes and data;

(4) (6) Performing the criticality safety analyses, and documenting a description of the calculation method and the nuclear data used.

4.11. Determination of the Where practicable, during the development of the criticality safety assessment, the personnel performing the assessment should directly observe all relevant aspects of the process or activity being assessed, including (if possible) any relevant equipment, activities, and
4.12. Before the commissioning of a new facility or the start of a new activity, or before an existing facility or activity is modified or changed in a way that might have an impact on criticality safety, the following actions should be taken:

(a) An independent review should be performed to confirm the adequacy of the criticality safety assessment. The reviewer should be competent in criticality safety assessment, as well as having knowledge of the facility or activity concerned. The review should include, at a minimum, the validation of the calculation method, the methodology for performing the criticality safety assessment, and a demonstration of subcriticality of the design and procedures during operational states and during credible abnormal conditions. The reviewer should also confirm that all credible abnormal conditions have been identified.

(b) The supervisor should verify that the scenarios described in the criticality safety assessment are appropriate, and that the criticality safety assessment adequately identifies all associated operational states and credible abnormal conditions.

**Defining the reference fissile material**

4.10.4.13. The characteristics of the reference fissile material (e.g. mass, volume, moderation, medium required for criticality safety assessment (see para. 6.144(a) of SSR-4 [2])) should be determined, justified, and documented. These characteristics include moderator nuclide composition, enrichment, (including physical form and chemical form (e.g. oxide, nitrate)), absorber depletion, degree of nuclide decay or in-growth, and interaction, irradiation (transmutation of fissile material, results of radioactive decay) be determined, justified and documented, and fission products. Estimates of the normal range of these characteristics, including conservative or bounding estimates of any anticipated variations in the characteristics, should be determined, justified and documented.

**Determination of the activity-processes and operations involving the fissile material**

4.11.4.14. The operational limits and conditions of involving the fissile material should be determined. A description of the operations being assessed should be provided, which should include all relevant systems, processes and interfaces. To provide clarity, this should include administrative systems, for example non-destructive testing and understanding, the systems for accounting for and control of materials. The description of the operations should be substantiated accompanied by relevant drawings, illustrations and/or graphics, as well as operating procedures.

4.12.4.15. The limits and conditions of each operation involving the fissile material should be
determined. Any assumptions made about the operations, and any associated systems, processes and interfaces that, which could impact the criticality safety assessment should be pointed out/identified and justified. Such systems include, but are not limited to, administrative systems, for example non-destructive assay, systems for accounting for and control of materials, and control of combustible material.

4.13.4.16. If the criticality safety assessment is limited to a particular aspect of a facility or activity, the potential for interactions with other facilities, systems, processes or activities should be described and considered.

Methodology  Defining the methodology for conducting the criticality safety assessment

4.14.4.17. The criticality safety assessment is expected to identify all credible initiating events, i.e. all incidents that could lead to an anticipated operational occurrence or a design basis accident (or the equivalent). These credible abnormal conditions. These initiating events should then be analysed and documented with account taken of possible aggravating events. Additionally, a justification is required for any identified initiating events that are excluded from the assessment: see para. 6.64 of SSR-4 [2]. The following should be considered when performing the analysis:

(a) All credible scenarios should be identified. A structured, disciplined and auditable approach should be used to identify credible initiating events. This approach should also include a review of lessons learned from previous incidents, including accidents, and also take into account the results of any physical testing. Techniques that can be used to help identify credible scenarios include, but are not limited to, the following:

   — “What-if” or cause–consequence methods;
   — Qualitative event trees or fault trees;
   — Hazard and operability analysis (HAZOP);
   — Bayesian networks;
   — Failure modes and effects analysis (FMEA).

(b) Input into the criticality safety assessment should also be obtained from the safety analysis report for the facility or activity, and from operating personnel and process specialists who are thoroughly familiar with the operations and initiating events that could credibly arise.

4.15.4.18. The criticality safety assessment be performed by using a verified and validated methodology. The criticality safety assessment provides a documented technical basis that demonstrates that subcriticality will/can be maintained in operational states and in design basis accidents (or the equivalent) credible abnormal conditions, in accordance with the double contingency principle or the single failure approach criterion (see paras. 3.7–3.11). The aim of the criticality safety assessment
is to identify the safety measures necessary to ensure subcriticality, and. The assessment should specify their safety functions, including requirements for of these safety measures, as well as criteria for the reliability, redundancy, diversity and independence, and also any requirements for of these measures. The equipment qualification criteria for these safety measures should also be specified.

4.16.4.19. The criticality safety assessment should describe the methodology or methodologies used to establish the operational limits and conditions for the activity being evaluated. Methods that may be used for the establishment of these limits and conditions include, but are not limited to, the following:

(a) Reference to national and international standards;
(b) Reference to accepted handbooks on criticality safety;
(c) Reference to experiments, with appropriate adjustments of limits to ensure subcriticality when the uncertainties of associated with the parameters reported in the experiment documentation are considered;
(d) Use of validated calculation models and techniques.

4.17.4.20. The applicability of the reference data used in the criticality safety assessment to the system of fissile material being evaluated should be justified. When applicable, any The calculation methods, computer codes and nuclear cross-section data used should be specified (i.e. cross-section data sets and including their release versions), together with any cross-section pre-processing codes that were used by assessors.

4.18.4.21. The overall safety assessment for the facility or activity should also be reviewed and used to identify and provide information on initiating events that should be considered as credible initiators of criticality accidents, for example, activation of sprinklers, rupture of a glovebox, buildup of material in ventilation filters, collapse of a rack, movement of fissile material during package transport and natural phenomena.

Verification and validation of the calculation methods and verification of nuclear data

4.22. Calculation methods such as involving the use of computer codes and an associated nuclear data library used in the criticality safety analysis to calculate \( k_{\text{eff}} \) are required to be verified and validated to ensure the reliability of their derived values to establish their limits of applicability, and acceptable levels of code bias and level of uncertainty.

4.23—Verification of the calculation methods should be performed prior to validation and periodically.
thereafter. Verification is the process of determining whether a calculation method correctly implements
the intended conceptual model or mathematical model

4.19.4.23. Verification of the calculation methods should be performed periodically and should test the methods, mathematical or otherwise, used in the model and for computer codes, and should ensure while ensuring that changes in the operating environment, i.e. operating system, software and hardware, do not adversely affect the execution of the codes.

4.4.4.4. The results of the calculations should be cross-checked by using independent nuclear data or different computer codes when available.

4.24. After verification of the calculation method is complete and prior to its use in performing a criticality safety analysis, the method should be validated. Validation relates to the process of determining whether the overall calculation method adequately reflects the real system being modelled, and enables the quantification of any calculation code bias and uncertainty, by comparing the predictions of the model with observations of the real system of fissile material or with evaluated experimental data [2]. The calculation method should be validated against selected benchmarks that are representative of the system being evaluated.

4.20.4.25. The relevance of benchmarks for use derived from experimental data in performing validation validating the criticality safety analysis should be determined from a comparison of the characteristics of the benchmarks with the characteristics of the system of fissile material being evaluated. A useful source of benchmark data can be found in Ref. [22].

4.21.4.26. In selecting benchmarks, consideration should be given to the following:

(a) Benchmarks should be used reviewed to ensure that information is complete and fully addresses stated biases and uncertainties before their use as benchmarks. Benchmarks should have known and relatively small uncertainties compared with any arbitrary or administratively imposed safety margin.

(b) Benchmarks should be selected from multiple independent sets in order to reduce the effect of shared benchmark uncertainties (e.g. correlations, leading to systematic effect uncertainties).

(b)(c) Benchmarks should be reviewed to ensure that their neutronic, geometric, physical and chemical characteristics encompass the characteristics of the system of fissile material to be evaluated. Examples of neutronic, geometric, physical or chemical characteristics are determined on the basis of system specifications that should be used for all materials include, but are not limited to, the following:

(i) Chemical compounds, mixtures, alloys and their compositions or formulae.

(ii) Isotopic proportions compositions.
(iii) Material densities.

(iv) Relative proportions or concentrations of materials, such as the moderator to fissile nuclide ratio. Effective moderators are typically materials of low atomic mass. Common materials that can be effective moderators include water (i.e. hydrogen, deuterium and oxygen), beryllium, beryllium oxide and graphite (i.e. carbon). In the presence or absence of poorly well-absorbing materials, nuclides, another element such as oxygen in magnesium oxide, oxygen, can be an effective moderator.

(v) The degree of homogeneity or heterogeneity and uniformity or non-uniformity, including gradients, of fissile and non-fissile materials (e.g. spent fuel rods, the settling of waste fissile materials such as waste in irradiated fuel rods);

(vi) Geometric arrangements and compositions of fissile material relative to non-fissile material such as neutron reflectors and including materials contributing to the absorption of neutrons (e.g. cadmium, boron, hafnium and gadolinium are commonly used, but other materials such as iron also act as slow neutron absorbers);

(vii) The sensitivity of the system to any simplification of geometry, for example elimination of pipes or ducts;

(vii) Temperature of the system;

(viii) Relevant neutron reflectors;

(ix) Neutron energy spectrum and spectrum index;

(x) Correlations between effective neutron multiplication factors due to nuclear data uncertainties.

Calculation methods should be reviewed periodically to determine whether relevant new benchmark data have become available for further validation.

Calculation methods should also be re-verified following changes to the computer code system and periodically thereafter.

4.3. Once the calculation method has been verified and validated, it should be managed within a documented quality assurance programme as part of the overall management system. The quality assurance programme should ensure that a systematic approach is adopted in designing, coding, testing and documenting the calculation method.

Criticality safety analyses

4.27. If no benchmark experiments exist that encompass representative of the system being evaluated (as may be the case, e.g. for low moderated powders and waste), it may be
possible to interpolate or extrapolate from other existing benchmark data to that system, by making use of trends in the bias. Where the extension from the benchmark data to the system at hand is large, the method should be supplemented by other calculation methods to provide a better estimate of the bias, and especially of its uncertainty in the extended area (or areas), and to demonstrate consistency of the computed results. An additional margin might be necessary to take into account for validation uncertainties in this case. Sensitivity analysis and uncertainty analysis may be used to assess the applicability of benchmark problems to the system being analysed and to ensure an acceptable safety margin. An important aspect of this process is the quality of the basic nuclear data and of the benchmarks. Comparison of the results from one computer code with the result from another computer code might be used to supplement the validation of a calculational method; however, this does not by itself constitute adequate validation.

4.28. The calculation methods, analysis techniques and nuclear data used in the evaluation of the applicability of benchmarks should be the same as those used to analyse the system or process to which the validation is applied; otherwise justification should be provided for the use of different techniques.

4.29. Appropriate statistical methods should be used to establish bias and bias uncertainty during the validation process (e.g. single-sided lower tolerance limit, single-sided lower tolerance band, single-sided lower confidence band). For cases involving data that is not normally distributed, a non-parametric approach may be appropriate.

Performing and documenting the criticality safety analyses

4.30. In the performance of criticality safety analyses, the calculation method should only be used within its validated area(s) of applicability; alternatively, any use of the calculation method outside of its area(s) of applicability should be documented and justified.

4.31. An additional subcritical margin (i.e. administrative margin) should be used to bound any unknown (or difficult to quantify) uncertainty beyond that identified in the validation, and the additional margin should be reasonable.

4.32. The $k_{eff}$ subcritical limit (sometimes referred to as the upper subcritical limit) should be established on the basis of the bias and bias uncertainty of the calculation method, the administrative margin, the features of the system and any related issues (e.g. use of the calculation method outside of its area(s) of applicability, the degree of experimental uncertainty) and considering the conservatism of the assumptions of the calculation models. When comparing the calculated $k_{eff}$ values with this subcritical limit, the remaining uncertainties in the data of the calculated $k_{eff}$ values (e.g. statistical uncertainties in Monte Carlo calculations) are required to be considered: see para 6.144(j) of SSR-4 [2].

4.33. When computer codes are used in the analysis, the type of computing platform,
(i.e. hardware and software) together with relevant information on the control of code configuration, especially calculation schemes, should be documented.

4.24.4.34. Quality control of management in relation to the input data and the calculation results is an important part of criticality safety analysis. This includes, for example, verification that Monte Carlo calculations have properly converged. All input data and nuclear data used in calculations, the assumptions, approximations and simplifications used to prepare the input data and the associated uncertainties, as well as the derived results and their uncertainties (see para 4.31), should be documented as part of the management system (see paras 2.17–2.21).

4.35. Once the calculation method has been verified and validated, it should be controlled and documented as part of the management system to ensure that a systematic approach is adopted.

4.36. The results of the calculations should be cross-checked by using independent nuclear data or different computer codes when available.

4.37. Benchmark modelling performed by organizations other than that performing the validation should be compared to confirm that the results are consistent.
5. CRITICALITY SAFETY FOR SPECIFIC PRACTICES

GENERAL

5.1. Criticality safety concerns many areas of the nuclear fuel cycle, for example, enrichment, fuel fabrication, fuel handling, transport and storage, reprocessing of spent fuel, and processing of radioactive waste and its disposal.

5.2. The facilities and activities of the nuclear fuel cycle can be split into two groups: those for which there is a potential for criticality hazard is not credible, and those for which there is no potential for criticality, for example, as follows:

(a) There is no potential for criticality in facilities for; mining of natural uranium and thorium ores and their processing, transport and conversion of natural uranium; and facilities;

(b) The potential for which the criticality hazards may be credible, for example, exists in enrichment facilities, uranium and mixed oxide fuel fabrication facilities, fresh fuel storage facilities, spentirradiated fuel storage facilities, reprocessing facilities, waste processing facilities and disposal facilities. Facilities in this second group should be designed and operated in a manner that ensures subcriticality in operational states and in design basis accidents (or the equivalent) transport of nuclear material.

1.24 The scope and level of detail to be considered for the criticality safety assessment the type of and its operation

SPECIFIC PRACTICES

5.2-5.3. This section provides recommendations on specific issues that should be taken into account to ensure criticality safety in each of the main areas of different practices in the nuclear fuel cycle. In all these practices, rigorous control of the physical inventory of fissile material is expected. Consequently, the potential for criticality resulting from errors such as over-batching, or the addition of water to vessels thought to be empty, should be eliminated: see para. 9.85(a) of SSR-4 [2].

CONVERSION AND CRITICALITY SAFETY IN URANIUM CONVERSION AND ENRICHMENT

5.4. Specific requirements for criticality safety in the operation of uranium conversion and enrichment facilities are established in para. 9.88 of SSR-4 [2].
In conversion facilities, typically natural uranium concentrates are purified and converted to the chemical forms required suitable for further steps in the manufacture of nuclear fuel — usually uranium tetrafluoride or uranium hexafluoride — if enrichment is needed. Because of the isotopic composition of natural uranium (i.e. approximately 0.7\% $^{235}$U by weight), in the homogeneous processes of conversion, and in the absence of enriched uranium or moderators more effective than water, no criticality safety hazards are encountered in the conversion of natural or depleted uranium.

Uranium enrichment facilities have the potential for criticality accidents; consequently, criticality safety measures, as described in the previous sections Sections 2 and 3, should be applied. Further guidance on

Before any wet cleaning of equipment or cylinders, an operational limit for uranium holdup should be defined, and it should be verified that the uranium holdup is below this limit.

Particular consideration should be given to criticality safety for conversion facilities and uranium enrichment facilities is provided in Ref. [19].

that are used for the conversion of enriched or reprocessed uranium, which has a higher enrichment than natural uranium and under certain conditions can achieve criticality.

Fuel fabrication facilities process powders, solutions, gases and solids of uranium and/or plutonium that might have different content in terms of either fissile material (e.g. in $^{235}$U or $^{239}$U enrichment) or absorber material (e.g. gadolinium).

Such facilities can be characterized by content for their fissile uranium content (for
uranium fuel fabrication or for facilities mixing powders of uranium and plutonium (i.e. or for mixed oxide fuel fabrication facilities) by the isotopic composition of the plutonium in the mixture (principally $^{239}$Pu, $^{240}$Pu and $^{241}$Pu), by the fissile fraction of plutonium (i.e. $(^{239}$Pu + $^{241}$Pu)/(total Pu) as a measure of plutonium quality), and by the fissile content in the uranium and by the mass fraction of PuO$_2$ in the total amount of oxides (i.e. the PuO$_2$ concentration).

5.6.5.14. A typical control parameter used in fuel fabrication is moderation. Where moderator control is employed, the following should be considered in the criticality safety assessment:

(a) Buildings containing fissile material should be protected from inundations of water from internal sources (e.g. from firefighting systems, leaks or failure of pipework) or ingress of water from external sources (e.g. rainfall and flooding).

(b) In order to prevent water leakage into fissile material, or fissile material leakage into water, and unexpected changes in conditions of criticality safety control, air rather than water should be used avoided as the heating and cooling medium in facilities for fissile material storage or processing. If this is not practicable, measures to limit the amount of water that can leak should be considered.

(c) For firefighting, procedures should be provided to ensure the safe use of fire extinguishing media (e.g. control of materials and densities of materials to be used, such as CO$_2$, water, foam, dry powders and sand). Combustible materials should be minimized in moderator controlled areas in order to reduce the likelihood of introducing moderating materials due to firefighting. Moderator control requirements should be specified in firefighting procedures. See also para. 6.146(c) of SSR-4 [2].

(d) The storage of fissile material should be designed to prevent its inadvertent rearrangement in events such as firefighting with high pressure water jets.

(e) Powders may absorb moisture. The maximum powder moisture content that could be reached from contact with humid air should be taken into account in the criticality safety analysis. If necessary, inert and dry glovebox atmospheres should be maintained to ensure the criticality safety and quality of packaged powders. Furthermore, the application of hydrogenated materials — for example, (e.g. materials used as lubricants in the manufacture of pellets) — should be applied with safety factors consistent with the double contingency principle. Criticality safety analyses for these types of material may be difficult to carry out on account of the limited number of experimental benchmarks that can be used in validating computer codes. Consequently, care should be taken in the extrapolation of available benchmark data for these applications. Guidance on such situations is provided in types of material (see also para. 4-27).

(f) The introduction and removal of moderating material — for example, under operational states and credible abnormal conditions (e.g. equipment or cleaning material, within moderator
controlled environments, such as in gloveboxes, packaging areas or criticality controlled areas
— should be monitored (e.g. by weighing moderating material) and controlled to avoid unsafe accumulations of moderated fissile material.

(g) The properties of all existing materials that could impact moderator content (e.g. hydric, hygroscopic, adsorptive, absorptive, and radiolytic properties).

(h) The spatial distribution of moderators within fissile material units, and the potential for non-uniform distribution due to chemical, thermal, or mechanical (e.g. mixing) processes.

(i) The tolerance to changes in the physical and chemical properties of moderators.

(j) The integrity of containers that are used to store and transfer moderating materials in moderator controlled areas.

(k) Moderating material that might be encountered during maintenance, decontamination, construction, and other activities.

5.7.5.15. Buildings and equipment (e.g. gloveboxes) should be designed to ensure the safe retention of fissile material in the event of a credible earthquake or other external event. Similarly, multiple separated systems relying on distance or neutron absorbers should be suitably fixed in place to ensure that an appropriate distance separation is maintained between them and to ensure the integrity of the neutron shielding.

5.8.5.16. The generation and collection of waste throughout the fuel fabrication process should be identified and evaluated to ensure that the quantities of fissile nuclides in any waste remain within specified limits.

5.17. Material Moderator controlled areas should be clearly identified to personnel.

5.18. Penetrations into moderator controlled areas should be minimized. Systems that normally contain moderating material, as well as systems that do not normally contain moderating material, and which penetrate a moderator controlled area should be considered.

**Fissile material cross-over**

5.9.5.19. Production Fuel production operations may be intermittent. To ensure adequate control during and between fuel production campaigns, the fundamental fissile material parameters that should be monitored include the mass of fissile material in each container, including the identification of the container (e.g. manipulated powders or pellets) and/or the identification of fuel rods and fuel rod assemblies. These identifications should ensure that the movement and storage
of these items is traceable, prevent unnoticed carry-over between batches and that the containers and workstations remain subcritical.

**Machining, grinding and cutting of fissile material**

5.10-5.20. The different steps in the manufacturing process may create accumulations of fissile material that might not be readily visible. In accordance with para. 9.84 of SSR-4 [2], a surveillance programme is required to be developed and implemented to ensure that uncontrolled accumulations of fissile material are detected, and further accumulation is prevented. A method for periodic cleaning and for accounting for and control of fissile material at the facility and at workstations should be defined that allows the identification and recovery of the fissile material. For credible accumulations of fissile material that are not readily visible, a method for estimating and tracking these residues should be developed to ensure that the workstations and ancillary systems remain subcritical. Such methods could involve quantification using spectral measurements, such as gamma spectrometry, or using a structured evaluation that estimates the volume of accumulated fissile material, with account taken of the contents and the densities of the material. These methods should take into account operating experience, previous interventions both internal and recording of information external. Consideration should be given to the possibility of entrainment of fissile material in process equipment or ancillary systems including ventilation systems due to the velocity of the transport medium. Periodic inspection of equipment in which fissile material could accumulate may be necessary.

5.11-5.21. Machining, grinding and cutting of fissile material should ideally be undertaken without the use of coolants. However, it might not be possible to eliminate coolants entirely from the process or to replace them with non-moderating coolants. The collection of accumulated residues and/or coolant is likely to necessitate control of other parameters, in particular the control of favourable geometry.

5.12-5.22. Further guidance on criticality safety for uranium fuel fabrication facilities and uranium and plutonium mixed oxide fuel fabrication facilities is provided in IAEA Safety Standards Series Nos SSG-6, Safety of Uranium Fuel Fabrication Facilities [23], and SSG-7, Safety of Uranium and Plutonium Mixed Oxide Fuel Fabrication Facilities [24].

**Handling and storage of fresh fuel**

5.13-5.23. The storage area for fresh fuel should comply with the conditions specified in the criticality safety assessment and should be such that the stored fresh fuel will remain subcritical at all times, even in the event of credible internal or external flooding or any other event considered credible in the design safety assessment. Engineered and/or
administrative measures should be taken to ensure that fuel is handled and stored only in authorized locations in order to prevent a critical configuration from occurring. It should be verified that the fissile material nuclide composition complies with the criticality limitations of the storage area.

5.14-5.24. For wet and dry storage systems that use fixed solid neutron absorbers, a surveillance programme should be put in place established to ensure that the absorbers are installed, and, if degradation of the absorbers is predicted, to monitor their effectiveness, and to ensure that they have not become displaced.

5.25. Drains in dry storage areas for fresh fuel should be properly kept clear to ensure the efficient removal of any water that might enter, so that such drains cannot constitute a possible cause of flooding.

5.26. Fire risks in the fuel storage area should be minimized by preventing the accumulation of combustible material in the storage area. Instructions for firefighting and firefighting equipment suitable for use in the event of a fire involving fuel should be readily available.

5.27. Further guidance recommendations for ensuring criticality safety in the handling and storage of fresh fuel at nuclear power plants is and at research reactors, are provided in IAEA Safety Standards Series Nos DS497D, Core Management and Fuel Handling for Nuclear Power Plants [25], and NS-G-4.3, Core Management and Fuel Handling for Research Reactors [26], respectively.

SPENT CRITICALITY SAFETY IN SPENT FUEL OPERATIONS (PRIOR TO BEFORE REPROCESSING, LONG TERM STORAGE OR DISPOSAL)

5.28. Spent fuel operations are generally characterized by a need to handle large throughputs and to retain large inventories of fissile material in the facility. Some of the recommendations provided for spent fuel (i.e. after final removal from the reactor core) may also be applied to any irradiated fuel handled and stored at the reactor site (i.e. before final irradiation in the reactor core). In determining the criticality safety measures, the following factors should be noted considered:

(a) The overall nuclide composition (including the fuel cycle, the material is highly radioactive isotopic composition of specific elements) and will generally need to be handled remotely in shielded facilities or shielded packages.

(b) Much of the material will need cooling (e.g. in spent fuel ponds) for several years following its removal from the reactor.

(c) The physical and chemical composition forms of the fissile material will have changed during irradiation in the reactor and subsequent radioactive decay. The effects of these changes on criticality safety (e.g. in terms of potential consequences, subcriticality margins and emergency preparedness and response) should be considered.
(b) The preferred method of ensuring subcriticality during spent fuel operations should be by means of geometrically favourable configuration of the fuel. Additional means, such as neutron absorbers and/or the use of a burnup credit, could be applied where subcriticality cannot be sufficiently or reliably maintained by means of favourable geometrical configurations alone. The effects of irradiation do not alter the preference for geometrically safe fuel storage.

(c) Spent fuel is highly radioactive and will need to be handled remotely in shielded facilities or shielded packages. This affects the potential consequences of a criticality accident by reducing the direct radiation exposure, although the energy release might increase the amount of contamination.

(d) Spent fuel will need cooling (e.g. in spent fuel pools) for several years following its removal from the reactor. The rate of change in fuel composition can be significant during this cooling period and the subcriticality margin is affected by such composition change.

(d)(e) The fuel assemblies will have undergone physical changes during irradiation.

Handling accidents

(f) The most reactive composition and geometry of irradiated fuel inside the reactor core is often not the most reactive composition and geometry of fuel in operations outside the reactor core. The radioactive decay after irradiation could lead to a significant increase of the effective neutron multiplication factor compared to the effective neutron multiplication factor derived from the nuclide composition at the end of the irradiation.

Events during the handling of spent fuel

5.19.5.29. The need for remote handling and the presence of heavy shielding necessary for radiation protection necessitates consideration of a set of credible abnormal conditions in which there is a potential for damage to fuel elements assemblies (e.g. leading to a loss of geometry control) or damage to other structures (e.g. leading to a loss of fixed absorbers). The safety measures associated with prevention of such conditions include the robust design of supporting structures, engineered and/or administrative limits on the range of movement of fuel elements assemblies and other objects in the vicinity of fuel elements assemblies, and regular testing and/or maintenance of handling equipment. Further recommendations on handling equipment are provided in SSG-15 (Rev. 1) [27].

5.30. Events during the handling of spent fuel might not lead directly to criticality; however, the potential for criticality in subsequent operations (e.g. transfer from a dry environment to a well-moderated environment) should be considered. Arrangements to check for and document any potential damage (e.g. to fissile material, absorber materials), for example before transfer from dry to wet handling of the spent fuel, should be made.
Maintaining spent fuel geometry

§5.20-5.31. Wherever it is necessary to maintain the geometry of irradiated fuel, it has to be maintained during storage and handling operations to ensure subcriticality, and this criticality safety should be assessed for operational states and for design basis accidents (or the equivalent) credible abnormal conditions. This includes the handling and storage of any degraded fuel (e.g., fuel with failed cladding) that has been stored in canisters. Water retention (even temporary) within these canisters after their removal from water should be considered. The potential for dispersion of fuel due to degradation of fuel cladding, or due to failures of fuel cladding or fuel assembly structures, should be assessed and included in the criticality safety assessment. Control over fuel geometry might also be affected by corrosion of structural materials and by embrittlement and creep of the fuel as a result of irradiation, and the potential for these effects should also be assessed. In some operations, for example in a dry environment, the geometry is not essential for ensuring subcriticality.

§5.21-5.32. For stored fuel there is sometimes a need to remove or repair fuel pins or rods, which can change the moderation ratio of the fuel element assembly and thus potentially increase its reactivity \( k_{\text{eff}} \) value. Criticality safety assessments should be performed to consider the impact of such operations.

Loss of soluble or fixed absorbers

§5.22-5.33. In some storage ponds pools for spent fuel, one possible criticality safety measure is the inclusion of a soluble neutron absorber (e.g., boron) in the storage pond pool water. In this case, the potential for accidental dilution of the soluble neutron absorber by unplanned additions of unpoisoned water not containing absorbers (or with lower concentration of absorbers) should be considered in the criticality safety assessment. Further guidance on safety of spent nuclear fuel storage is provided in [...].

§5.23-5.34. Fixed absorber materials used in spent fuel pools should be designed so that high radiation fields levels do not lead to detrimental changes in their physical and chemical form. In existing facilities where ageing of neutron absorbers has already occurred, the fixed absorber materials used as a criticality safety measure. For example, Boraflex sheets (a material composed of boron carbide, silica, and polydimethyl siloxane polymer) used in some storage ponds solid neutron absorbers for pressurized water reactor and boiling water reactor spent fuel have been found to shrink as a result of exposure to radiation, creating gaps in the material and reducing the effectiveness of the neutron absorbers certain credible abnormal conditions, such as a drop of a fuel assembly should be given only limited credit. In accordance with Requirement 32 of SSR-4 [2], the ageing degradation of neutron absorbers throughout the lifetime of the facility should be considered, to ensure that their physical integrity remains consistent with the assumptions used in the safety analysis.

§5.24-5.35. The potential for degradation of criticality safety measures involving soluble or fixed...
absorbers should be included in the criticality safety assessment. Safety measures associated with events of this type may include restrictions on the volume of water that could cause accidental dilution, periodic sampling and measurement of levels of soluble neutron absorbers, and periodic inspection and/or surveillance of fixed absorber materials. Sampling of soluble boron in the pond water should be carried out in such a manner as to verify that the level of boron is homogeneous across the pond. Where soluble boron is used as a criticality safety measure, operational controls should be implemented to maintain water conditions in accordance with specified values of temperature, pH, redox, activity, and other applicable chemical and physical characteristics, so as to prevent boron dilution. Additionally, appropriate measures to ensure boron mixing by, for example, thermal convection caused by decay heat in the storage pond should be taken into account. Where boron solutions are stored outdoors in a cold climate, the potential for boron separation due to freezing and thawing should be considered.

Changes in storage arrangements within a spent fuel facility

Spent fuel is often stored in pond facilities for several years following its removal from the reactor core. During that time, changes may need to be made to the storage configuration. For example, in some nuclear power plants it has been found necessary to reposition the spent fuel in the storage pond, that is, to ‘re-rack’ the spent fuel, in order to increase the storage capacity of the pond. Increasing the density of fuel storage have significant effects on the level of neutron absorption necessary to ensure subcriticality. A reduction in the amount of interstitial water between spent fuel assemblies in a storage rack may also cause a reduction in the effectiveness of fixed absorbers (see Ref. [13]). These effects should be taken into account in the criticality safety assessment for such modifications.

Consideration should also be given to the potential for changes in the storage arrangement due to credible abnormal conditions involving fuel movements or heavy equipment movements, e.g. a flask container being dropped onto the storage configuration.

Misloading

For events involving spent fuel facilities on a single reactor site where the facility may have more than one type of fuel element and/or have storage areas with different requirements for acceptable storage within the same facility, the possibility of misloading of a fuel into wrong storage should
also be considered in the criticality safety assessment.

5.27-5.38. Some spent fuel storage facilities accept material spent fuel from a range of reactor sites. To accommodate the different types of fuel, the facility is usually divided into areas with distinct design features and requiring different degrees of criticality safety measures. In these situations, the potential for misloading of spent fuel into the wrong storage location should be considered in the criticality safety assessment. Safety measures associated with events of this type should include engineered features to preclude misloading (e.g., based on the physical differences in fuel assembly design); alternatively, administrative controls and verification of the fuel assembly markings should be applied.

5.39. The preventive safety measures for misloading events should include engineered features to preclude misloading (e.g., that might occur due to the physical differences in fuel assembly design), and administrative controls and verification of the fuel assembly markings.

Taking account of changes in spent fuel composition as a result of irradiation

5.40. In some criticality safety assessments for operations involving spent fuel fuel that is (or will be) irradiated, the spent fuel has been conservatively assumed to have the same composition with the maximum effective neutron multiplication factor (sometimes called the ‘peak reactivity’). For many types of fuel, the peak reactivity is achieved by fresh fuel. For other types of fuel there is a peak in reactivity at a higher irradiation level (burnup) for at least two reasons, as follows:

(a) The buildup of new fissile nuclides from fertile nuclides is more significant than the depletion of the initial fissile nuclides;

(b) The effect of the depletion of integral burnable absorber nuclides (usually gadolinium isotopes) within the fuel composition is stronger than the effect of the depletion of fissile nuclides, leading to a net increase in the effective neutron multiplication factor. Taking account of the burnable absorber is referred to as burnable absorber credit (or gadolinium credit when that absorber is involved).

5.41. The maximum effective neutron multiplication factor due to irradiation should be taken into account, except in the following cases:

(a) The fuel, which might have a maximum above zero irradiation (burnup), can be demonstrated as not being irradiated; or

(a)(b) It can be sufficiently demonstrated that the fuel has reached a minimum irradiation level (burnup) and that the effects of this burnup can be safely accounted for, taking credit for reductions in $k_{\text{eff}}$ as a result of changes in the spent fuel composition due to irradiation. This more realistic approach is commonly known as ‘burnup credit’, and can be applied instead of the ‘peak $k_{\text{eff}}$ approach’ (i.e.
peak reactivity achieved during irradiation), for which an assessment is required whenever \( k_{\text{eff}} \) could increase due to irradiation. The application of burnup credit is covered in paras. 5.45–5.48; see paras. 5.45–5.48.

5.28. Taking credit for burnable absorbers in fuel that may be irradiated does not involve verification of the burnup of individual fuel assemblies will increase the potential for misloading, should form one but does involve verification of the key considerations in the criticality safety assessment for spent-fuel operations.

5.28–5.42. Further guidance on criticality safety at spent-fuel storage facilities is provided in designs and guidance on ensuring subcriticality during the handling and storage of spent fuel at nuclear power plants is provided in Initial enrichment.

**Burnup credit**

5.29. The changes in the composition of spent fuel during irradiation will eventually result in a reduction in \( k_{\text{eff}} \). The application of burnup credit in the criticality safety assessment may present several advantages, as follows:

(a) Increased flexibility of operations (e.g. acceptance of a wider range of spent fuel types);

(b) Verified properties of the sufficiently irradiated fuel, possibly resulting in an inherently subcritical material;

(c) Increased loading densities in spent fuel storage areas;

(d) Larger capacity transport packages (casks);

(e) Burnup credit may also be applied to assessments of emergency conditions, leading to a more appropriate response planning.

5.44. Paragraph 6.148 of SSR-4 [2] states that “if the design of the facility takes into account burnup credit, its use shall be appropriately justified in the criticality safety analysis.”

5.30. The application of burnup credit may significantly increase the complexity, uncertainty and difficulty in demonstrating an adequate margin of subcriticality. The criticality safety assessment and supporting analysis should reliably determine the maximum value of \( k_{\text{eff}} \) for the system, by taking into account the changes to the fuel composition during irradiation and changes due to radioactive decay after irradiation. Spatial variations in the spent fuel composition should be taken into account in calculating \( k_{\text{eff}} \) for the relevant configuration of the spent fuel. The increase in complexity presents several challenges for the criticality safety assessment. In a criticality safety assessment carried out on the basis of burnup credit, the following should be addressed:
(a) Validation of the calculation methods used to predict the spent fuel composition—see paras. 4–22–4.29.

(b) Validation of the calculation methods used to predict $k_{\text{eff}}$ for the spent fuel configurations—see paras. 4–22–4.29. Calculations for burnup credit in spent fuel may now include many more nuclides than are present for fresh fuel calculations; consequently, additional uncertainties in nuclear data and the conservatism applied should be justified.

(c) Specification and demonstration of a suitably conservative representation of the irradiation conditions, for example, the amount of burnup, the presence of soluble absorbers, the presence of burnable poison absorbers, coolant temperature and density, fuel temperature, power history and cooling time. For fuel assemblies with burnable poisons, the criticality safety assessment should take account of the depletion of burnable poisons and should consider the possibility that the most reactive condition may not be for the fresh fuel.

(d) Justification of any modelling assumptions, for example, the representation of smoothly varying changes in composition (i.e. as a result of radial and axial variations in burnup) as discrete zones of materials in the calculation model.

(e) Justification of the inclusion or exclusion of specific nuclides such as fission products, of the ingrowth of fissile nuclides and of the loss of neutron absorbers.

5.31.5.46. Generally, the operational limits and conditions for ensuring subcriticality in spent fuel storage on the basis of an assessment of burnup credit are based on a conservative combination of the fuel’s initial enrichment of the fuel and the accumulated burnup history (in which the amount of burnup is an important parameter), credible fuel history variations are taken into account) for each fuel type. This approach is commonly known as the ‘safe loading curve’ approach (see Ref. H[27]). In such circumstances, the criticality safety assessment should determine the operational measures necessary to ensure compliance with this curve during operation; for example, the measurements that are necessary to verify the initial enrichment and burnup. The criticality safety assessment should also consider the potential for misloading of fuel from outside the limits and conditions specified in the safe loading curve.

5.47. Without applying burnup credit, there might be a large number of different fuel designs that necessitate individual administrative controls. For cases in which credit is taken for the burnup of individual fuel assemblies, sequences involving fuel misloading should be specifically considered at reactor sites where fuel at different burnup levels, including fresh fuel, are handled. Screening of received

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16 The safe loading curve joins pairs of values of initial enrichment and burnup that have been demonstrated to be safely subcritical.
fuel assemblies can reduce the potential for misloading events where burnup credit is applied (a very small fraction of fuel assemblies are typically outside the allowable range and can be accounted for individually by special measures). Protection against misloading events, as described in paras. 5.38 and 5.39, should form one of the key considerations in the criticality safety assessment for spent fuel operations.

Further information and guidance on the application of burnup credit is available in Ref. [29].

CRITICALITY SAFETY IN FUEL REPROCESSING

Reprocessing

1.29 facilities recover the uranium and plutonium from spent fuel by removing waste products (e.g. cladding, fission products, and minor actinides) from the fuel assemblies after it has been irradiated.

Reprocessing operations can also include the treatment of fresh fuel, fertile material or low burnup fuel. Specific consideration should be given to specific criticality safety measures for controlling the dissolution phase, since fresh fuel or low burnup fuel can be more difficult to dissolve than spent fuel. In addition, uranium and plutonium mixed oxide fuels tend to be more difficult to dissolve than UO₂ fuels, and Th bearing fuels exhibit complicated dissolution behavior.

Specific requirements for criticality safety in the design of facilities handling mixed uranium and plutonium liquids are established in para. 6.153 of SSR-4 [2], and specific requirements for the operation of fuel reprocessing facilities are established in para. 9.89 of SSR-4 [2].

The following issues are of particular importance and should be considered for criticality safety in reprocessing facilities:

(a) The wide range of forms of fissile material involved in reprocessing, potentially making the use of multiple control parameters necessary.

(b) Variations in neutron fluxes and spectra caused by other actinides than uranium and plutonium.

(c) The mobility of solutions containing fissile nuclides and the potential for their misdirection.

(d) The need for chemistry control in order to prevent the following:

   (i) Precipitation, colloid formation and increases of concentration in solution;

   (ii) Unplanned separation and extraction of fissile nuclides.

(e) The possibility for holdup and accumulations of fissile material owing to incomplete dissolution of materials, accumulation of fissile material in process equipment (e.g. conditioning and vacuum vessels) or ventilation systems, or chronic leaks (including leaks of liquors onto hot surfaces).
The need for moderator control during furnace operations causing condensation in powders.

Wide difficulties in monitoring the continuous processes in operations with high radiation levels.

The wide range of forms of fissile material in fuel reprocessing facilities

5.35, 5.52. The criticality safety considerations for reprocessing facilities should include the following different forms of fissile material involved in reprocessing are diverse and could include, as applicable:

(a) Fuel assemblies;
(b) Fuel rods;
(c) Sheared fuel;
(d) Fines or swarf;
(e) Solutions of uranium and/or plutonium;
(f) Oxides of uranium or plutonium, or mixed oxides of uranium and plutonium;
(g) Plutonium oxalate or mixed uranium and oxalate and plutonium oxalate;
(h) Uranium or plutonium metals;
(i) Other compositions (e.g. materials containing minor actinides).

Mobility of solutions and the potential for their misdirection in fuel reprocessing facilities

5.36, 5.53. Many fissile materials are in a liquid form and, because of the existence of many connections between items of equipment, the possibility for misdirection of the fissile material should be considered in the criticality safety assessment. The criticality safety assessment should be such as to identify the safety measures necessary to avoid this possibility, for example, the use of overflow lines and siphon breaks. Misdirection can lead to uncontrolled chemical phenomena (e.g. concentration or precipitation of plutonium or dilution of neutron absorbers in solution) or misdirection of fissile material to systems of unfavourable geometry. The potential for misdirection is required to be taken into account in the criticality safety assessment: see para. 6.146(a) of SSR-4 [2]. The criticality safety assessment should identify the safety measures necessary to avoid misdirection; for example, the use of overflow lines and siphon breaks.

5.37, 5.54. The criticality safety assessment should give particular consideration to the impact of interruptions to normal operations (e.g. owing to corrective maintenance work) that have the potential to create unplanned changes to the flow of fissile material. The possibility that external connections could
be added in an ad hoc unsystematic manner to approved pipework and vessels should also be considered.

Operational experience has shown that misdirection of fissile material can occur owing to unexpected pressure differentials in the system (e.g. due to sparging operations during cleanup). The criticality safety assessment should include consideration of these effects.

In any facility employing chemical processes, leaks are a constant hazard. Leaks might occur as a result of faulty welds, joints or seals, etc. Ageing of the facility might also contribute to leaks through corrosion, vibration and erosion effects. Leaks and the effects of corrosion, erosion and vibration are required to be taken into account in the criticality safety assessment: see para. 6.146(b) and (d) of SSR-4 [2]. In general, drains, drip trays, recovery pans and vessels of favourable geometry should be provided to ensure that any fissile materials that could leak will be safely contained. Consideration should also be given to the provision of monitored sumps of favourable geometry for the detection of leaks. It should not be assumed that leaks will be detected in sumps, as they might evaporate and form solid accumulations over time. Consideration should be given to carrying out performing inspections to prevent any long term buildup of fissile material, especially in areas where personnel are not present (see Ref. [29]).

Maintaining chemistry control in fuel reprocessing facilities

Particular consideration should be given to chemistry control during reprocessing. Some of the most important process parameters that could affect the criticality safety measures include: acidity, concentration and/or density, purity of additives, temperature, contact area (i.e. during mixing of materials), flow rates and quantities of reagents. Loss of control of any of these process parameters could lead to a range of unfavourable changes, for example such as the following:

(a) Increased concentration of fissile nuclides (by precipitation, colloid formation or extraction);
(b) Unplanned separation of plutonium and uranium;
(c) Carry-over of uranium and plutonium into the raffinate stream;
(d) Incomplete dissolution of fissile material.

The potential for such changes described in para. 5.57 to affect criticality safety should be considered in the criticality safety assessment. The selection of suitable safety measures will vary depending on the details of the process and may include the following:

(a) Monitoring of the concentration of fissile nuclides (e.g. in-line neutron monitoring, chemical

\[17\] A raffinate stream is the liquid stream that remains after the solutes from the original liquid are removed through contact with an immiscible liquid.
sampling); (b) Monitoring of flow rates and temperatures; (c) Testing of acidity and quality control of additives.

The effectiveness and reliability of these safety measures that are applied should be considered as part of the criticality safety assessment. The process flowsheet\(^{18}\) required by para. 6.153 of SSR-4 [2] helps in determining the response and sensitivity of the facility to changes in the process parameters, control parameters, and safety parameters. This information should be used to ensure that the safety measures applied are able to respond quickly enough to detect, correct or terminate unsafe conditions in order to prevent a criticality accident. Time lags in process control should be considered in maintaining chemistry control.

Particular consideration should be given to the control of restart operations following interruptions to normal operating conditions. Some changes in chemical characteristics may occur during any period of shutdown (e.g. changes in the valence state of plutonium leading to a reduction in acidity, which could result in formation of colloids), and these effects should be accounted for in re-establishing a safe operating state.

**Holdup and accumulation of fissile material in fuel reprocessing facilities**

Paragraph 9.84 of SSR-4 [2] states:

“Depending on the potential for criticality arising from accumulations of fissile material, including waste and residues, a surveillance programme shall be developed and implemented to ensure that uncontrolled accumulations of fissile material are detected and further accumulation is prevented.”

In a reprocessing facility there are many sites where fissile material may accumulate and many mechanisms (both physical and chemical) by which fissile material could be diverted from the intended process flow. In addition, owing to the high throughput of material, these losses may be hard to detect solely on the basis of material accounting.

The start of the reprocessing operation usually involves mechanical operations, such as shearing and/or sawing of the fuel to facilitate its dissolution. Such operations are usually conducted in a dry environment, and so the risk of criticality will often be lower than in a wet environment. However, particular consideration should be given to the possibility of accumulations of fissile nuclides.

\(^{18}\) A process flow sheet depicts a chemical or operational engineering process and describes the materials, rates of flow, volumes, concentrations, enrichments and masses necessary to attain intended results or products.
in swarf, fines and other debris becoming moderated through entrainment during subsequent parts of the process with wet chemistry conditions. For this reason, regular inspections and housekeeping should be carried out performed as part of the surveillance programme. See also para. 3.21.

5.45-5.63. The next mechanism process by which accumulation could occur is dissolution. Incomplete dissolution may might occur as a result of a range of credible abnormal conditions; for example, low acidity, low temperature, short dissolution time, overloading of fuel and low acid volume. Criticality safety measures to be considered should include, but are not limited to, the following:

(a) Pre-dissolution control on the conditioning of acids;
(b) Monitoring of temperature and dissolution time;
(c) Post-dissolution monitoring for gamma radiation (e.g. to detect residual undissolved fuel in hulls);
(d) Controls on material balance;
(e) Density measurements.

5.46-5.64. The effectiveness, reliability and accuracy of these safety measures described in para. 5.64 should be considered as part of the criticality safety assessment. In particular, the possibility that sampling may might not be representative should be considered. Similarly, the potential for settling of fine particles of fissile material in the bottom of vessels throughout subsequent processes should also be considered. In these cases, neutron monitoring of the lower parts of vessels and periodic emptying and flushing of vessels may should be necessary considered.

5.47.5.65. The potential for fissile nuclides to remain attached to cladding following dissolution should be considered. For example, in some cases residual plutonium can bond to the inside surface of cladding as a result of polymerization.

5.48.5.66. Recommendations to trap on trapping and monitoring leaks in equipment with favourable geometry and to provide monitored sumps to detect such leaks are provided in para. 5.5. However, it is possible that very slow leaks or leaks onto hot surfaces, (i.e. the material crystallizes before reaching the measuring point, may might occur. Such losses of material can be very difficult to detect. Safety measures for events of this type may such leaks should include, but are not limited to, periodic inspections of the areas below vessels and pipework, and the review of operational records to identify such any chronic loss of fissile material. The criticality safety assessment should consider the timescales over which unsafe accumulations of fissile material could occur so that suitable inspection frequencies can be determined.

Moderator control in furnace operations in fuel reprocessing facilities

5.49.5.67. For most furnace operations carried out as that are part of the conversion process (e.g. 64
precipitation, drying, oxidation), it may be practicable to use vessels with favourable geometry should be considered. It may also be practicable to ensure that the internal volume of the furnace has a favourable geometry. However, the oxide powders produced in subsequent operations may require moderation control to allow feasible storage arrangements. The conversion process should be designed such that it does not lead to the production of material with excessive moderator content. The criticality safety assessment should therefore consider mechanisms by which the moderator might be carried over (e.g. incomplete drying) or introduced (e.g. condensation during cooling).

5.68. Further recommendations on criticality safety in reprocessing facilities are provided in IAEA Safety Standards Series No. SSG-42, Safety of Nuclear Fuel Reprocessing Facilities [30].

CRITICALITY SAFETY IN RADIOACTIVE WASTE MANAGEMENT

5.69. Waste management operations cover a very wide range of facilities, processes and materials. The recommendations in paras 5.71–5.78 apply to packaging, storage and disposal operations involving fissile material. The recommendations are also intended to apply to legacy waste. Waste management operations, particularly in a disposal facility, may involve large inventories of fissile material from a wide range of sources. In the case of legacy waste, there might also be considerable variation in and uncertainty about the waste properties (e.g. the physical form and chemical composition of the non-fissile and fissile components of the waste). In contrast, decommissioning operations typically involve small inventories of fissile material.

Waste management and decommissioning

5.50, 5.70. The collection and storage of unconditioned radioactive waste before its processing should be made subject to the same considerations in the criticality safety assessment as the processes from which the waste was generated. (see also paras 9.84 and 9.85 of SSR-4 [2]). Additionally, special considerations may be necessary if such waste streams are mixed with other radioactive waste streams of different origin or if the individual inventories of fissile material before processing are generally small, significant accumulations of such material may occur in the subsequent waste collection and waste processing steps.

5.51. Waste management operations cover a very wide range of facilities, processes and materials. The following recommendations apply to packaging, interim storage and disposal operations. The recommendations are intended to cover the long term management and disposal of waste arising from

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operations involving fissile material (e.g. ‘legacy waste’). Waste-management operations may be shielded or unshielded and may involve remote or manual handling operations. Management operations, particularly in a disposal facility, involve large inventories of fissile material from a wide range of sources. In the case of legacy waste, there may also be considerable variation in and uncertainty about the material properties (e.g. in the physical form and chemical composition of the non-fissile and fissile components of the waste material). In contrast, decommissioning operations typically involve small inventories of fissile material.

5.52. Waste is commonly wrapped in materials that can act as are more effective moderators than water — for example, (e.g. polyethylene or polyvinyl chloride) — and this should be taken into account in the criticality safety assessment.

5.53. Criticality safety for waste operations should be determined on the basis of the application of appropriate limits on the waste package contents. Criticality safety measures may include the design of the packages (see para. 9.85(c) of SSR-4 [2]) and the arrangements for handling, storage and disposal of many packages within a single facility. Where practicable, package limits should be applicable to all operations along within the waste management route chain, including operations at the subsequent disposal facility, so that subsequent repacking, with its associated hazards, may be avoided. The future transport of the waste packages (see paras 5.81–5.88) should also be considered, so as to avoid the need to repack the waste to meet ensure compliance with the criticality safety requirements and other transport requirements established in SSR-6 (Rev. 1) [3].

5.54. For the storage of waste containing fissile nuclides, consideration should be given to potential changes in the configuration of the waste, the introduction of a moderator or the removal of material (such as neutron absorbers) as a consequence of a credible internal or external event (e.g. movement of the waste, precipitation of solid phases from liquid waste, loss of confinement of the waste, a seismic event). Further recommendations are provided in IAEA Safety Standards Series No. WS-G-6.1, Storage of Radioactive Waste [32]. When it is necessary to prevent the settling of fissile material to maintain a subcritical configuration, the method used should be passive. Such situations can arise in long term storage (or, e.g., during the separation of fissile solids from aqueous mixtures).

5.55. Assessment The assessment of criticality safety for the period after the closure of a disposal facility presents particular challenges. These include the need to consider the effects of geochemical and geophysical processes on the disposal facility over very long timescales be considered. Following the closure of a disposal facility, engineered barriers provided by the package design and the form of the waste will tend to degrade, allowing the possibility of separation, relocation and accumulation

\[^{20}\text{Legacy waste is radioactive waste that may contain fissile material that has remained from historic fissile material facilities and past activities that (a) were never subject to regulatory control or (b) were subject to regulatory control but not in accordance with the requirements of the International Basic Safety Standards [26].}\]
In addition, a previously dry environment might be replaced by a water saturated environment. Consideration of the consequences of criticality after closure of a disposal facility will differ from that for, for example, fuel stores or reprocessing plants, where a criticality accident might have immediate recognizable effects. In the case of a disposal facility, disruption of protective barriers and effects on transport mechanisms of radionuclides are likely to be more significant than the immediate effects of direct radiation from a criticality event, because the radiation produced by such an event would be shielded by the surrounding host rock formation and/or backfill materials.

5.56. In the criticality safety assessment of waste management operations, consideration should be given to the specific details of the individual facilities and processes involved. Consideration should be given to the following particular characteristics of waste management operations with respect to criticality safety:

(a) The nuclear, radiological, physical and chemical properties of the waste as parameters for waste classification;

(b) Variation and uncertainty in the form and composition of the waste; (see para 5.76);

(c) The need to address the degradation of engineered barriers and the evolution of waste packages after emplacement over long timescales; (see para. 5.77);

(d) Criticality safety requirements and other transport requirements to facilitate future transport of the waste. (see paras 5.81–5.88).

Variation and uncertainty in waste forms

5.57. Variation and uncertainty in waste forms is a particular challenge for some types of legacy waste for which the accuracy and completeness of historical records might be limited. Therefore, criticality safety assessments for legacy waste to be disposed of should be performed in a comprehensive and detailed manner. If conservative deterministic methods are applied, in which bounding values are applied to each material parameter, the resulting limits on packages might prove to be very restrictive. This might then lead to an increase in the number of packages produced, resulting in more handling and transport consignments and higher storage volumes, each of which is associated with a degree of risk (e.g. radiation doses due to operating personnel occupational exposures, road or rail accidents, construction accidents). Therefore consequently, particular consideration should be given to optimization of the margins to be used in the criticality safety assessment. If an integrated risk approach is used, consideration should be given to the balance of risk between the criticality hazard and the other hazards.
Degradation of engineered barriers over long timescales

5.58.5.77. With regard to the disposal of spent fuel, the fissile inventory of spent fuel mainly consists of any remaining $^{233}$U and/or $^{235}$U and the plutonium isotopes $^{239}$Pu and $^{241}$Pu. Over the very long timescales considered in post-closure criticality safety assessments, some reduction and change in the fissile inventory of the nuclear waste will occur owing to radioactive decay. However, such criticality safety assessments should also take into account of credible degradation of the engineered barriers of waste packages, with consequential relocation and accumulation of fissile and non-fissile components.

Decommissioning

TO ACCOUNT FOR CRITICALITY SAFETY IN DECOMMISSIONING

5.59.5.78. In the assessment of criticality safety during decommissioning, a graded approach should be applied that takes into account the type of facility and therefore the fissile inventory present. Generally, this Safety Guide should be applied if fissile material in relevant amounts is handled, so that criticality safety needs to be considered. Additional guidance and recommendations on the decommissioning of nuclear fuel cycle facilities are provided in IAEA Safety Standards Series No. SSG-47, Decommissioning of Nuclear Power Plants, Research Reactors and Other Nuclear Fuel Cycle Facilities [33].

5.60.5.79. Before beginning decommissioning operations, any accumulations of fissile material should be identified in order to assess the possibilities for recovery of this material. Consideration should be given to the potential for sites with unaccounted for accumulations of fissile material (e.g. active lathe sumps). A method for estimating and tracking accumulations of fissile material that are not readily visible should be developed to ensure that workstations remain subcritical during decommissioning operations, (see also para. 9.84 of SSR-4 [2]). This method should take into account operating experience, any earlier interventions to remove fissile material, recorded information and any records of physical inventory differences, process losses and/or measured holdup. The estimation of such accumulations of fissile material could be based on quantification using spectral measurements (e.g. gamma spectrometry) or by a structured evaluation of the volume of material, with account taken of the contents and densities of the material.

5.61.5.80. The approach used to ensure subcriticality in decommissioning may be similar to that used for research laboratory facilities (see paras. 5.89–5.96), where setting a low limit on allowable masses of fissile material provides the basis for allowing other parameters (e.g. geometry, concentration, moderation, absorbers) to take any value. In accordance with para. 7.4 of IAEA GSR Part 6 [7], an initial decommissioning plan for a facility is required to be developed and submitted to the regulatory body together with the application for authorization to operate the facility design and construction, and it be...
This initial decommissioning plan is required to be maintained during facility operation and updated, in accordance with Requirement 10 of GSR Part 6 [7]. When a facility approaches its permanent shutdown, a final decommissioning plan is required to be prepared; see Requirement 11 of GSR Part 6 [7]. In facilities handling significant amounts of fissile material, consistent with the graded approach, all decommissioning plans should be supported by criticality safety assessments, in order to ensure that practices carried out in the operating lifetime and activities performed during the operation of the facility do not create avoidable problems later in decommissioning.

TRANSPORT OF CRITICALITY SAFETY IN THE TRANSPORT OF FISSION MATERIAL AND DURING THE ON-SITE MOVEMENT OF FISSION MATERIAL

5.62-5.81 Movement or transfer of radioactive material within a licensed site should be considered to be on-site. Requirements for the safe transport of radioactive material off the site (i.e. in the public domain), including consideration of the criticality hazard, are established in recommendations - SSR-6 (Rev. 1) [3]. Recommendations to support these requirements are provided in SSG-26 [10], TS-G-1.4 [21] and IAEA Safety Standards Series No. TS-G-1.5, Compliance Assurance for the Safe Transport of Radioactive Material [34].

5.63-5.82 Although the established in SSR-6 (Rev. 1) [3] provide a prescriptive system for package subcriticality design assessment, they are not entirely free of: however, engineering judgement. Often is still needed, especially for estimating the potential behaviour of a package under accident conditions, of transport, for which considerable engineering expertise is required. Consequently, this assessment. The criticality safety assessment for transport should therefore be carried out only by persons with suitable knowledge and experience of the transport requirements.

5.64-5.83 The assessment of subcriticality referred to in para. 5.82 provides a safety basis, but the transport conditions comply with the requirements set forth in for the package design approval. Reference 4 In addition, a criticality safety assessment for the transport of such packages under real conditions is required in accordance with para. 673 of SSR-64 (Rev. 1) [3], which states that:

"Fissile material shall be transported so as to:
(a) Maintain subcriticality during routine, normal and accident conditions of transport; in particular, the following contingencies shall be considered:

(i) Leakage of water into or out of packages;

(ii) Loss of efficiency of built-in neutron absorbers or moderators;

(iii) Rearrangement of the contents either within the package or as a result of loss from the package;

(iv) Reduction of spaces within or between packages;

(v) Packages becoming immersed in water or buried in snow;

(vi) Temperature changes.\(^{21}\)

1.32 Hazards to be considered for on-site transfer should include, but are not limited to, the following:

5.84. Provisions: The state of a prototype transport package before, during and after the tests specified in SSR-6 (Rev. 1) \(^{[3]}\) (e.g. water spray and immersion, drop and thermal tests) can provide confirmation of the assumptions made for the criticality assessment and analysis of the design. Since the tests should verify the assumptions used in the criticality safety analysis, many tests need to be considered to cover each scenario (e.g. an individual package and a package in an array configuration).

5.85. The criticality safety assessment of a transport package, complying with a package design approved for off-site transport in accordance with the requirements of SSR-6 (Rev. 1) \(^{[3]}\) may rely upon this approval for the use in a facility. In such a case, it should be demonstrated that all operational states and credible abnormal conditions in a facility are bound by the existing transport package design safety assessment.

5.86. The following should be considered with regard to the on-site movement of fissile material:

(a) Measures to ensure that packages of fissile material remain reliably fixed to vehicles;

(b) Vehicular speeds and road conditions;

(c) Potential interactions with other fissile material that may come close in transit on the site.

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\(^{21}\) In the context of the Transport Regulations, fissile material as defined in para. 222 of SSR-6 (Rev. 1) \(^{[3]}\) includes only \(^{233}\)U, \(^{235}\)U, \(^{239}\)Pu and \(^{241}\)Pu, subject to a number of exceptions \(^{[6]}\). Other fissile nuclides may need to be taken into account in a criticality safety assessment.
5.65. There are some research and development laboratories that utilize fissile material in sufficient quantities such that there is a potential for criticality. These facilities are generally characterized by the need for high flexibility in their operations and processes, but typically have low inventories of fissile material and can include hands-on direct handling and/or remote handling operations. The general assumption of low inventories that there is only a small inventory of fissile material might not be applicable for laboratories that are used for fuel examinations or experiments, or their respective waste treatment facilities.

5.88. Access to a wide range of fissile and non-fissile materials in research and development laboratories are established in paras 6.154–6.156 of SSR-4 [2].

The range of fissile and non-fissile materials in research and development laboratories

5.89. The research and development nature of laboratory operations, laboratories can use a wide range of fissile and non-fissile materials and separated elements and nuclides, typically including low, intermediate and high enriched uranium, plutonium that is high in $^{241}$Pu content (e.g. >15 wt.%), plutonium that is low in $^{240}$Pu content (e.g. <5 wt.%), graphite, boron, gadolinium, hafnium, heavy water, zirconium, pore former, aluminium and various metal alloys. Examples of special fissionable (including fissile) and non-fissile fissionable nuclides sometimes encountered include $^{233}$U, $^{237}$Np, $^{242}$Pu, $^{241}$Am, $^{242m}$Am, enriched boron (e.g. $^{10}$B) and enriched lithium (e.g. $^{6}$Li). These nuclides have diverse energy dependent nuclear reaction properties (e.g. neutron fission, neutron absorption, neutron scattering, gamma neutron reaction and gamma fission properties), which can result in non-linear and seemingly incongruent variations of critical mass. Should therefore

5.66. Materials containing significant quantities and concentrations of the nuclides referred to in para. 5.89 should receive specific consideration in the criticality safety assessments and analyses. Useful references for determining the properties of some of these include Refs [35, 36]. Particular challenges are encountered in determining the critical mass of unusual materials that contain significant fractions of special nuclides (e.g. $^{241}$Cm, $^{244}$Cm), because often there are few criticality experiment benchmarks with which $k_{eff}$ computations with these nuclides and materials can be validated.

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22 Pore former is an additive that is used in the blending of nuclear fuel oxides for the purpose of creating randomly distributed closed pores in the blended oxide prior to pelletizing and sintering for the purpose of producing pre-sintered fuel pellets that are free of flaws and have improved strength. Pore former has a neutron moderating effect.
Overlap of operating criticality controlled areas and interfaces between materials in research and development laboratories

5.67.5.91. Owing to the significant flexibility in operations, criticality safety measures are applied to the location and movement of fissile material within the laboratory laboratories are important in ensuring subcriticality. Any associated limits and conditions should be specified in the criticality safety assessment. The criticality safety assessment should define criticality controlled areas and should specify their limiting content and boundaries and the maximum content of fissile material, and any other associated limits and conditions.

5.68.5.92. Particular consideration should therefore be given to the potential for any overlap of these criticality controlled areas and any interfaces between materials in such overlaps. The management system (see paras 2.17–2.40) should ensure that the combining of material from another different criticality controlled area or areas and the movement of moderators into a criticality controlled area is restricted and that any such combining or movement is subject to a criticality safety assessment before it is carried out.

Inadverted consolidation of fissile material in research and development laboratories

5.69.5.93. Frequently, activities in a specific laboratory area may be interrupted to perform a different operation. In such cases, laboratory operating personnel should exercise particular care to avoid any unanalysed or unauthorized inadvertent accumulation of fissile material that could occur as a result of housekeeping or consolidation of materials, prior to admitting more fissile and non-fissile materials into the laboratory area.

Specialized education and training of operating personnel in research and development laboratories

5.70.5.94. Because of the diverse characteristics of materials and laboratory operations, laboratory operating personnel and management should be appropriately educated and trained about the seemingly anomalous be provided with specific training on the characteristics of typical and special fissile material and non-fissile materials under different degrees of neutron moderation.

Additional information

1.33. Particular challenges will be encountered in determining the critical mass of unusual materials, such as some of those listed in para. 5, and other exotic trans-plutonium materials (e.g. $^{243}$Cm, $^{245}$Cm), because frequently there are no criticality experiment benchmarks with which criticality computations

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with these materials can be validated.
Planning for Subcritical Assemblies

5.95. Subcritical assemblies are generally used for research and educational purposes. Subcritical assemblies have the potential for criticality accidents; hence, criticality safety measures should be applied. Annex II of IAEA Safety Standards Series No. SSR-3, Safety of Research Reactors [37] provides an overview of the application of the safety requirements to subcritical assemblies.
6. **EMERGENCY PREPAREDNESS AND RESPONSE TO A CRITICALITY ACCIDENT**

6.1. This provides recommendations on emergency response (EPR). Requirements for preparedness and response to a nuclear or radiological emergency are established in GSR Part 7 [9]. Associated recommendations and guidance are provided in IAEA Safety Standard Series Nos GSG-2, Criteria for Use in Preparedness and Response for a Nuclear or Radiological Emergency [38], GS-G-2.1, Arrangements for Preparedness for a Nuclear or Radiological Emergency [39], GSG-11, Arrangements for the Termination of a Nuclear or Radiological Emergency [40], and DS469, Preparedness and Response for a Nuclear or Radiological Emergency Involving the Transport of Radioactive Material [41].

6.2. Priority should always be given to the prevention of criticality accidents by means of defence in depth. Despite all the precautions that are taken in the handling and use of fissile material, there remains: however, there is always a possibility that a failure (i.e. of instrumentation and controls, or an electrical, mechanical or operational error) or an event may give rise to a criticality accident. In some cases, this may give rise to such an accident might result in exposure of persons to direct radiation (neutron and gamma) and/or a release of radioactive material within the facility and/or to the environment, either of which may necessitate emergency response actions. Adequate preparations are required to be The kinetic energy release from a criticality accident could also result in considerable non-radiological hazards.

**GENERAL CONSIDERATIONS FOR EMERGENCY PREPAREDNESS AND RESPONSE TO A CRITICALITY ACCIDENT**

6.3. Requirement 1 of GSR Part 7 [9] states:

> “The government shall ensure that an integrated and coordinated emergency management system for preparedness and response for a nuclear or radiological emergency is established and maintained at the local and national levels, and, where agreed between States, at the international level, for response to a nuclear or radiological emergency [8, 33, 34].”

This management system should also cover criticality accidents, as appropriate. The government is also required to make provisions to ensure that the roles and responsibilities for preparedness and response to such an emergency are clearly assigned: see Requirement 2 of GSR Part 7 [9].

6.4. In accordance with Requirement 4 of GSR Part 7 [9], the government is required to perform a hazard assessment. This hazard assessment is required to consider criticality accidents, including events of very low probability not considered in the design, and combinations of events and emergencies: see para 4.20 of GSR Part 7 [9].
6.5. The development of the protection strategy based upon the hazard assessment and potential consequences of an accident, in accordance with Requirement 5 of GSR Part 7 [9], should consider the possible deterministic effects (evaluated on the basis of relative biological effectiveness weighted absorbed dose) as well as stochastic effects (evaluated on the basis of equivalent dose).

For each facility in which fissile material is handled and for which a criticality detection and alarm system is required (see para. 6.149(a) of SSR-4 [2]) an emergency plan, procedures and capabilities to respond to foreseeable criticality accidents are also required (see Requirement 72 of SSR-4 [2a]). In some circumstances where a criticality detection and alarm system is not installed (e.g.,

**CAUSES AND CONSEQUENCES OF A CRITICALITY ACCIDENT**

6.6. shielded facilities; see para. 6.36 (c)), analyses should still be conducted to determine whether an emergency plan is necessary for the facility.

6.6.7. In demonstrating the adequacy of the emergency arrangements, the potential occupational exposures and, if relevant, the dose to a member of the public external exposure exposures (see Para 6.150 of SSR-4 [2]) should be calculated / estimated. The analysis of the potential consequences of a criticality accident should consider the criticality events that have occurred at similar facilities elsewhere (see Table 1 of GSR Part 7 [9]).

**FUNCTIONAL CONSIDERATIONS FOR EMERGENCY PREPAREDNESS AND RESPONSE TO A CRITICALITY ACCIDENT**

6.8. In accordance with para. 5.17 of GSR Part 7 [9], the government is required to ensure that appropriate arrangements are in place for the following:

(a) To promptly recognize and classify an emergency caused by a criticality accident. The operational criteria for classification are required to include emergency action levels and other observable conditions and indicators: see para. 5.16 of GSR Part 7 [9].

(b) To promptly declare the emergency class and to initiate a coordinated and pre-planned on-site response.

(c) To notify the appropriate notification point and to provide sufficient information for the initiation of an effective, coordinated and pre-planned off-site response, if needed.

6.9. Arrangements are required to be in place to mitigate the consequences of a criticality accident; see Requirement 8 of GSR Part 7 [9]. Possible approaches include the installation of isolation valves, remote control systems (e.g., for ensuring the availability of neutron absorbers and the means of introducing them into the system where the criticality has occurred), portable shielding or other means of safely
altering the process conditions to achieve a safe state.

6.10. Consideration should be given to limiting or terminating radioactive releases by shutting down facility ventilation systems in the event of a criticality accident. The possibility of an increase in hydrogen gas concentration due to radiolysis if such measures are implemented should also be considered.

6.11. In some accidents, incorrect actions by operating personnel have inadvertently initiated a further criticality event after the initial event. It should be ensured that operating personnel are aware that following the initial fission spike(s), the system might return to a state that is very close to critical but with a continuing low fission rate. This typically occurs in systems containing solutions in which inherent negative reactivity feedback effects offset the excess reactivity inserted in the initial stages of the event. In such situations, very small additions of reactivity could be sufficient to initiate further fission spikes.

6.12. The main risk in a criticality accident is to operating personnel in the immediate vicinity of the event. Generally, radiation doses to operating personnel more than a few tens of metres away are not life threatening. However, it is common for some normally sufficient to cause severe deterministic effects; however these radiation doses can still be significant, and appropriate escape routes and assembly points are required to be provided: see para. 6.149(b) of SSR-4 [2]). Some types of system, particularly fissile nuclides in solution, can display oscillatory behaviour with multiple bursts of radiation continuing over hours or even days. Because of this, a key element in emergency planning should be to ensure prompt notification and evacuation of persons to a safe distance. Following this, sufficient information should be gathered to enable a planned re-entry to the facility. (see paras 6.29–6.32).

6.13. The radiation dose from provision of additional shielding should also be considered as a means of minimizing the radiological consequences of a criticality accident. The effects of any penetrations through the shielding should be evaluated. When planning additional shielding for people located at some distance from the accident. Thus, a mechanism criticality accidents, priority should be given to escape routes for operating personnel.

6.14. Emergency procedures should designate escape routes for persons on the site. These routes should be clearly indicated. Evacuation should follow the quickest and most direct routes practicable, with consideration given to the need to minimize radiation exposure. Any changes to the facility should not impede evacuation or otherwise lengthen evacuation times. Identifying appropriate evacuation and the emergency procedures should stress the importance of speedy evacuation. Recommendations for re-entry to the facility are provided in paras. 6.29–6.32.

6.15. Personnel assembly points should be designated outside the areas to be evacuated, with appropriate consideration given to nuclear security (see para. 2.6) and the need to optimize radiation exposures. Means should be provided for confirming that all personnel have been evacuated from the area in which the criticality event has occurred.
6.16. Para. 5.52 of GSR Part 7 [9] states:

“The operating organization and response organizations shall ensure that arrangements are in place for the protection of emergency workers and protection of helpers in an emergency for the range of anticipated hazardous conditions in which they might have to perform response functions.”

Guidance values for restricting the exposure of emergency workers are provided in Appendix 1 of GSR Part 7 [9]. Appropriate equipment, including personal protective equipment (where appropriate) and radiation monitoring equipment, including personal dosimeters, capable of measuring the radiation emitted during a criticality accident should be provided to emergency workers. Further guidance on the use of criticality dosimeters is provided in para. II.50 of IAEA Safety Standards Series No. GSG-7, Occupational Radiation Protection [42].

Managing the medical response in the event of a criticality accident

6.17. Arrangements for managing the medical response in the event of a criticality accident are required to be in place, in accordance with Requirement 12 of GSR Part 7 [9]. This includes the pre-designation of medical facilities with a trained and multidisciplinary healthcare team, to provide specialized treatment for individuals exposed to a criticality event. Recommendations on medical follow-up are provided in GSG-11 [40].

6.18. The data and information to be gathered for the medical management of affected individuals should include basic contact details, information on the circumstances under which the criticality accident occurred, and any relevant medical history (e.g. previous illnesses, co-morbidities, habits).

6.19. Reconstructing the dose distribution in the human body is critical to the medical response. Paragraph 5.102 of GSR Part 7 [9] states:

“Arrangements shall be made to document, protect and preserve, in an emergency response, to the extent practicable, data and information important for an analysis of the nuclear or radiological emergency and the emergency response.”

These arrangements should include comprehensive interviews with those involved on the circumstances of the criticality accident to help guide the emergency response.

Dose estimation for a criticality accident

6.20. The process of estimating the radiation dose from a criticality accident is subject to various uncertainties. The acceptable level of uncertainty (or the level of confidence that the dose is not greater than predicted) will be a decisive factor in determining the method to be used and the assumptions that can be made to produce the estimate.
6.21. The initial estimation of the dose from a criticality accident should consider, at a minimum, the following:

(a) The location of the criticality accident;

(b) The power history of the criticality accident (i.e. the number of fissions that have occurred as a function of time);

(c) The effect of any shielding (including the source of the criticality itself) between the location of the criticality system and those likely to be affected (i.e. operating personnel);

(d) The individuals likely to be affected (i.e. operating personnel), and the orientation of their bodies in relation to the criticality accident;

(e) The neutron energy spectrum to which affected personnel were exposed;

(f) The equivalent doses to individual organs, in order to determine appropriate medical interventions.

6.22. It is possible that a clear picture of the location and cause of the accident might not emerge for several hours. Additional information may come from several sources (e.g. radiation monitors, eyewitness accounts, facility records). The following information should be used to refine the dose reconstruction:

(a) Details of the items of equipment involved;

(b) The radiological, physical and chemical properties of the fissile material, including quantities;

(c) The reactivity insertion mechanism that caused the system to achieve criticality;

(d) Feedback and quenching mechanisms\(^23\) present (such as venting);

(e) An estimation of any radioactive release (see Ref. [43]).

INFRASTRUCTURAL CONSIDERATIONS FOR EMERGENCY PREPAREDNESS AND RESPONSE TO A CRITICALITY ACCIDENT

6.23. Requirement 20 of GSR Part 7 [9] states that “\[t\]he government shall ensure that authorities for preparedness and response for a nuclear or radiological emergency are clearly established.” In addition, Requirement 24 of GSR Part 7 [9] states:

“The government shall ensure that adequate logistical support and facilities are provided to enable emergency response functions to be performed effectively in a nuclear or radiological emergency.”

\(^{23}\)A quenching mechanism is a physical process other than mechanical damage that limits a fission spike during a nuclear criticality excursion, for example, thermal expansion or micro-bubble formation in solutions [171313].
The authorities for preparedness and response to a criticality accident may be similar or identical to those established for other types of nuclear or radiological emergency.

6.24. Each response organization is required to prepare a specific emergency plan or plans for coordinating and performing their assigned functions: see para. 6.17 of GSR Part 7 [9]. In addition, the appropriate responsible authorities are required to ensure that a ‘concept of operations’ for the response to a criticality accident is developed, at the preparedness stage: see para. 6.18 of GSR Part 7 [9].

6.25. In accordance with Requirement 25 of GSR Part 7 [9], training, drills and exercises are required to be provided for personnel involved in the emergency response to a criticality accident, to ensure that such personnel are able to perform their assigned response functions effectively.

6.26. The response to criticality accidents might involve knowledge, skills and abilities beyond those needed for other nuclear and radiological emergencies, and this should be taken into account at the preparedness stage. References [14, 44, 45] provide detailed descriptions of the dynamic behaviour of criticality accidents that have occurred. The exercises for criticality accidents (see para. 6.25) could be developed on the basis of the descriptions of accidents in these references.

CAUSES AND STABILIZATION OF A CRITICALITY ACCIDENT

6.27. Of the 22 criticality accidents in nuclear fuel processing cycle facilities reported in Ref. [1], all but one [14], 21 involved fissile material in solutions or slurries. In these events (i.e. mixtures of enriched uranium or plutonium compounds with water or organic chemicals). The majority of the accidents were caused by an increase in concentration of fissile nuclides, which resulted from movement of fissile material by gravity or by flow through pipework. In these accidents, the key physical parameters affecting the fission yield (i.e. the total number of fissions in a nuclear criticality excursion) were the following:

(a) The mass of the fissile region (particularly for systems with fissile nuclides in solution).
(b) The reactivity insertion mechanism and reactivity insertion rate.
(c) Parameters relating to reactivity feedback mechanisms, for example:
   — Doppler feedback$^{24}$;
   — Duration time and time constant of reaction;

$^{24}$Doppler feedback is a phenomenon whereby the thermal motion of fissile and non-fissile material nuclei changes the ‘relative’ energy between the nuclei and interacting neutrons, thereby causing an effective broadening of neutron reaction cross-sections of the materials. Depending upon the enrichment or composition of the materials, this phenomenon can increase or decrease the effective neutron multiplication factor ($k_{\text{eff}}$) of a system.
— Degree of confinement of the fissile material;
— Neutron spectral shifts;
— Degree of voiding;
— Change of temperature;
— Density changes.

Special consideration should be given to plutonium solutions as positive temperature reactivity feedback can occur [46, 47]. Guidance on estimating the magnitude of the fission yield can be found in Refs. [48, 49].

6.4.6.28. Typically, criticality accidents in solution systems have been characterized by one or several fission excursion spikes\(^{25}\), particularly at the start of the transient, followed by a ‘quasi-steady state’ or plateau phase in which fission rates fluctuate much more slowly.

1.34 An assessment of 22 criticality accidents identified a common theme in terms of the reactivity excursion mechanism: the majority of the accidents were caused by an increase in concentration of fissile nuclides, which resulted from movement of fissile material by gravity or by flow through pipework. A detailed description of the dynamic behaviour in these criticality accidents can be found in Ref. [17].

**EMERGENCY PREPAREDNESS AND RESPONSE**

6.1. Each facility in which fissile material is handled and for which the need for a criticality detection and alarm system has been determined (see paras 6.49–6.51) should have in place an emergency response plan, programme and capabilities to respond to credible criticality accidents. In some circumstances where a criticality detection and alarm system is not installed (e.g., shielded facilities), analyses should still be conducted to determine whether an emergency response plan is necessary for the facility.

6.2. Evacuation of persons to a safe distance. The radiation dose from a criticality accident may still be significant, even for people located at some distance from the accident. Thus, a mechanism for identifying appropriate evacuation and assembly points should be developed.

6.3. The design should provide a diversity of communication systems to ensure reliability of communication under operational states and accident conditions.

\(^{25}\) A fission excursion spike is the initial power pulse of a nuclear criticality excursion event, limited by quenching mechanisms and mechanical damage [47,13].
6.4.—The provision for additional means of shielding should also be considered in minimizing the radiological consequences of a criticality accident. In employing shielding as a protective measure, the implications that penetrations through the shielding may have for radiation dose should be evaluated. When planning additional shielding measures (e.g., walls) for emergency cases, priority should be given to safe escape routes for operating personnel.

Emergency response plan

6.5.—In general, the emergency response plan specific to a criticality accident should include the following:

- Definition of the responsibilities of the management team and the technical personnel, including the criteria for notifying the relevant local and national authorities;
- Evaluation of locations in which a criticality accident would be foreseeable and the expected or possible characteristics of such an accident;
- Specification of appropriate equipment for use in a criticality accident, including protective clothing and radiation detection and monitoring equipment;
- Provision of individual personal dosimeters capable of measuring radiation emitted during a criticality accident;
- Consideration of the need for appropriate medical treatment and its availability;
- Details of the actions to be taken on evacuation of the facility, the evacuation routes and the use of assembly points;
- A description of arrangements and activities associated with re-entry to the facility, the rescue of persons and stabilization of the facility;
- Training, exercises and evacuation drills;
- Assessment and management of the interface between physical protection and criticality safety in a manner to ensure that they do not adversely affect each other and that, to the degree possible, they are mutually supportive.

Responsibilities

6.6.—Emergency procedures should be established and made subject to approval in accordance with the management system. Management should review and update the emergency response plan on a regular basis (e.g., owing to modifications in the facility operations or changes in the organization).
6.7—Management should ensure that personnel with relevant expertise are available during an emergency.

6.8—Management should ensure that organizations, including the emergency services, both on-site and off-site, that are expected to provide assistance in an emergency are informed of conditions that might be encountered and are offered training as appropriate. These organizations should be assisted by technical experts in preparing suitable emergency response procedures.

6.9—Management should conduct emergency exercises on a regular basis to ensure that personnel are aware of the emergency procedures and should conduct an awareness programme for local residents.

6.10—Management, in consultation with relevant staff for criticality safety, should specify the conditions and criteria under which an emergency is declared, and should specify the persons with the authority to declare such an emergency.

6.11—During an emergency response, the relevant staff for criticality safety should be available to advise and assist the nominated emergency coordinator in responding to the criticality accident.

6.12—The operating organization should have the capability to conduct, or should engage external experts to conduct, an assessment of radiation doses appropriate for a criticality accident.

Evaluation of foreseeable accidents

6.13—Locations at which a criticality accident would be foreseeable should be identified and documented, together with an appropriate description of the facility. The predicted accident characteristics should be evaluated and documented in sufficient detail to assist emergency planning. Such an evaluation of foreseeable criticality accidents should include an estimate of the fission yield and the likelihood of occurrence of the criticality.

6.14—In the design and operation stages and as part of periodic safety review, consideration should be given to identifying further measures to prevent a criticality accident and to mitigate the consequences of a criticality accident, for example, measures for intervention in order to stop the criticality. Possible approaches include the installation of isolation valves, remote control systems (e.g. for ensuring the availability of neutron absorbers and the means of introducing them into the system where the criticality has occurred), portable shielding or other means of safely altering the process conditions to achieve a safe state.

6.15—The process of calculating the radiation dose from a criticality accident is subject to various uncertainties. The final dose estimate will therefore also include uncertainty. The acceptable level of uncertainty (or the level of confidence that the dose is not greater than predicted) will be a decisive factor in determining the method to be used or the assumptions that can be made to produce the estimate. The methodology for determining the dose from a criticality accident is complex but should follow the following basic steps:
• Decision on the location of the criticality accident;
   (a) Decision on the power of the criticality accident (i.e. the number of fissions that have occurred);
• If desired, calculation of the effect of any shielding (including the source of the criticality itself) between the location of the criticality system and those likely to be affected (i.e. operating personnel);
• Calculation of the dose received by those likely to be affected (i.e. operating personnel).

6.16. The determination of the doses should be conservative, but not so conservative that it endangers personnel through measures such as unnecessary evacuation.

6.17. The emergency response plan should be implemented, consistent with the initial evaluation of the criticality accident.

Initial evaluation of the criticality accident

6.18. Information on the event will come from a number of sources (e.g. radiation monitors, eyewitness accounts, facility records), and it is possible that a clear picture of the location and cause of the accident may not emerge for several hours. The key information will be:
   (a) The location of the event, including details of the items of equipment involved;
   (b) The radiological, physical and chemical properties of the fissile material, including quantities;
   (c) The reactivity insertion mechanism that caused the system to achieve criticality;
   • Feedback and quenching mechanisms present (such as venting).

6.19. On the basis of this information, the relevant staff for criticality safety should make a reasonable prediction as to the likely evolution of the system with time and should advise the emergency response team on possible options for terminating the criticality and returning the system to a safe subcritical state.

6.20. Once the information listed in para. 6.26 is available, useful comparisons can be made with details available from other criticality accidents (see Refs [17, 36, 37]). This will help with predictions of the likely evolution of the current event and may also provide information as to possible methods to terminate the power excursion. In some cases termination may be achieved by reversing the reactivity insertion mechanism that initiated the criticality accident.

4.35. In some accidents, there have been instances where improper actions of operating personnel have inadvertently initiated a further power excursion after the initial criticality accident. It should be borne in

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26 A quenching mechanism is a physical process other than mechanical damage that limits a fission spike during a nuclear criticality excursion, for example, thermal expansion or micro-bubble formation in solutions [171313].
mind that following the initial fission spike(s), the system might return to a state at or very close to critical but with a continuing low fission rate. This typically occurs in solution systems in which inherent negative reactivity feedback effects will tend to balance out the excess reactivity inserted in the initial stages of the event. In such situations, very small additions of reactivity could then be sufficient to initiate further fission spikes.

**Instrumentation and equipment**

6.21. On the basis of the accident evaluation, provision should be made for appropriate protective clothing and equipment for emergency response personnel. This equipment could include respiratory protection equipment, anti-contamination suits and personal monitoring devices.

6.22. Emergency equipment (and an inventory of all emergency equipment) should be kept in a state of readiness at specified locations.

6.23. Appropriate monitoring equipment, for use to determine whether further evacuation is needed and to identify exposed individuals, should be provided at personnel assembly points.

**Evacuation**

6.24. Emergency procedures should designate evacuation routes, which should be clearly indicated. Evacuation should follow the quickest and most direct routes practicable, with consideration given to the need to minimize radiation exposure. Any changes to the facility should not impede evacuation or otherwise lengthen evacuation times.

1.36 The emergency procedures should stress the importance of speedy evacuation and should prohibit return to the facility (re-entry) without formal authorization.

6.25. Personnel assembly points, located outside the areas to be evacuated, should be designated, with consideration given to the need to minimize radiation exposure.

6.26. Means should be developed for ascertaining that all personnel have been evacuated from the area in which the criticality event has occurred.

6.27. The emergency procedures should describe the means for alerting emergency response personnel, the public and the relevant authorities.

**Re-entry, rescue and stabilization**

6.28. An assessment of the state of the facility should be conducted by nominated, suitably qualified and experienced staff relevant for criticality safety, with the support of operating personnel, to determine the actions to be taken on the site to limit radiation dose and the spread of contamination.
6.29. The emergency procedures should specify the criteria and radiological conditions on the site that would lead to evacuation of potentially affected areas and a list of persons with the authority to declare such an evacuation. If these areas could exceed the site limits, relevant information should be provided to off-site emergency services and appropriate information should be included in the emergency procedures.

6.30. Radiation levels should be monitored in occupied areas adjacent to the immediate evacuation zone after initiation of the emergency response. Radiation levels should also be monitored periodically at the assembly points.

6.31. Re-entry to the facility during the emergency should be allowed back into the facility during an emergency due to a criticality accident. Persons re-entering should be provided with personal dosimeters that monitor both gamma and neutron radiation.

6.32. Re-entry should be made only if radiological surveys indicate that the radiation levels are acceptable. Radiation monitoring should be carried out during re-entry using monitors that have an alarm capability.

6.33. The emergency response plan should describe the provisions for declaring the termination of an emergency, and the emergency procedures should describe the procedures for re-entry and the membership of re-entry teams. The operating organization should take the primary responsibility for the termination of an emergency due to a criticality accident (see Requirement 18 of GSR Part 7 [9] and the recommendations provided in GSG-11 [40]). Lines of authority and communication for the termination of the emergency should be included in the emergency procedures.

Medical care

6.34. Arrangements should be made in advance for the medical treatment of injured and exposed persons in the event of a criticality accident. The possibility of contamination of personnel should be considered.

6.35. Emergency planning should also include a programme for ensuring that personnel are provided with dosimeters and for the prompt identification of exposed individuals.

6.36. Planning and arrangements should provide for a central control point for collecting and assessing information useful for emergency response.

Training and exercises

6.37. References [17, 36, 37] provide detailed descriptions of the dynamic behaviour of criticality accidents that have occurred in the past. These references could be used to develop training exercises.
6.35. Relevant staff for criticality safety should familiarize themselves with publications on criticality accidents to ensure that learning from past experience is factored into criticality safety analyses and the emergency response plan.

CRITICALITY DETECTION AND ALARM SYSTEMS

6.32. If the emergency plan specifies the use of special material to shut down or stabilize the system, such as a neutron absorber, a sufficient quantity of the material should be available. The potential for corrective actions to make the situation worse (see para 6.10) and the hazards to emergency workers should be assessed before attempting corrective actions.

CRITICALITY DETECTION AND ALARM SYSTEMS

6.33. The need for a criticality detection and alarm system should be assessed for all facilities and activities involving, or potentially involving, the risk of criticality. In determining this, consideration should be given to all processes, including those in which neutron moderators or reflectors more effective than water may be present. See para. 6.149(a) of SSR-4 [2].

6.34. In determining the need for a criticality detection and alarm system, individual areas of a facility may be considered unrelated if the boundaries are such that there could be no inadvertent interchange of material between areas, and neutron coupling is negligible.

6.35. Where installed, the criticality detection and alarm system should provide effective information to minimize the total dose received by personnel from a criticality accident, and to initiate mitigating actions.

6.36. Justification of any exceptions to the need to provide a criticality detection and alarm system should be provided and could be based upon the following cases:

(a) Where a documented assessment concludes that no foreseeable set of circumstances could initiate a criticality accident, (see para. 6.173 of SSR-4 [2]), or where the provision of a criticality detection and alarm system would offer no reduction in the risk from a criticality accident or would result in an increase in total risk, that is, the overall risk to operating personnel from all hazards, including industrial hazards.

(b) Shielded facilities in which the potential for a criticality accident is foreseeable but the resulting radiation dose at the outer surface of the facility where the accident occurred would be lower than the acceptable level. (see para. 6.173 of SSR-4 [2]). Examples of such facilities might include hot cells and closed underground repositories.
(c) Licensed or certified transport packages\textit{Packages requiring competent authority approval} for fissile material awaiting shipment or transport, during shipment or transport, or awaiting unpacking.

6.12-6.37. Where the potential for criticality exists but no criticality alarm system is employed, another means to detect the occurrence of a criticality event should still be provided.

6.38. Facility personnel should be trained in the correct response to criticality detection and alarm system activation and deactivation.

\textbf{Performance and testing of criticality detection and alarm systems}

\textit{Limitations and general recommendations}

6.13-6.39. The criticality detection and alarm system should be based on the detection of is required to detect neutron and/or gamma radiation; see para. 6.172 of SSR-4 [2]. Consequently, consideration should be given to the deployment of detectors that are sensitive to both neutron radiation and gamma radiation or, or both. If applicable, other reliable and practical methods could be adopted.

\textit{Detection}


\begin{quote}
“Instrumentation and control systems used to ensure subcriticality shall be of high quality and shall be calibrated against known standards. Changes to computer codes and data shall be controlled to a high standard by means of the management system.”
\end{quote}

\textit{Criticality detection}

6.14-6.41. In areas in which criticality alarm coverage is necessary, means should be provided to detect excessive radiation doses and/or dose rates and to trigger an alarm for the evacuation of personnel.

\textit{Alarm}

\textit{Criticality alarms}

6.15-6.42. The alarm signal should meet the following criteria:

(a) It should be unique (i.e. it should be immediately recognizable to personnel as a criticality alarm);

(b) It should actuate as soon as the criticality accident is detected and continue until manually reset, even if the radiation level falls below the alarm point;

(c) Systems (with restricted access) to manually reset the alarm signal, with limited access, should be provided outside areas that require evacuation need to be evacuated;
(d) The alarm signal should be audible in all areas to be evacuated.

(e)(d) It should continue to alarm for a time sufficient to allow a complete evacuation;

(e) The alarm should be supplemented with visual signals in areas with high background noise.

**Dependability of criticality detection and alarm systems**

6.16.6.43. Consideration should be given to the need to avoid false alarms, for example, by using concurrent response of two or more detector channels to trigger the alarm. In the evaluation of the criticality detection and alarm system, consideration should be given to other hazards that may result from the triggering of a false alarm.

6.17.6.44. Criticality detection systems, without immediate evacuation alarms, should be considered for special situations where it is demonstrated that mitigating actions could be executed to automatically bring the system back to a safe state and to reduce the radiation dose to personnel.

6.18.6.45. Warning signals indicating a malfunction but not actuating the alarm should also be provided.

**Design criteria for criticality detection and alarm systems**

6.19.6.46. The design of the criticality detection and alarm system should be single failure tolerant and be as simple as is consistent with the objectives of ensuring reliable actuation of the alarm and avoiding false alarms.

6.20.6.47. The performance of the detectors should be carefully considered in order to avoid issues such as omission of an alarm signal or saturation of signals.

6.21.6.48. Uninterruptible power supplies should be available for the criticality detection and alarm system.

**Trip point**

**Trip points of criticality detection and alarm systems**

6.22.6.49. The trip point for the criticality detection and alarm system should be set sufficiently low to detect the minimum accident of concern, but sufficiently high to minimize false alarms. Indications should be provided to show which detector channels have been tripped.

**Positioning of the detectors in criticality detection and alarm systems**

6.23.6.50. The location and spacing of detectors should be chosen to minimize the effect of shielding by equipment or materials. The spacing of detectors should be consistent with the selected alarm trip
In the decommissioning of facilities, it is common practice to establish interim storage areas for items such as waste drums or to position modular containment systems around items of equipment requiring size reduction or dismantling. The implications of the location of such interim storage areas for the continuing ability of the criticality detectors to detect the minimum accident of concern should be subject to prior evaluation. The implications of the location of such interim storage areas for the continuing ability of the criticality detectors to detect the minimum accident of concern should be subject to prior evaluation.

**Testing of criticality detection and alarm systems**

The entire criticality detection and alarm system should be tested periodically. Testing periods should be determined from operating experience and should be kept under review. Performance testing of the criticality detection and alarm systems should include the periodic calibration of the radiation detectors used in the criticality detection and alarm systems.

Each audible signal generator should be tested periodically. Field trials Tests should be carried out to verify that the signal is audible above background noise throughout all areas to be evacuated. All personnel in affected areas should be notified in advance of a test of the alarm.

Where tests reveal a test indicates the inadequate performance of the criticality detection and alarm system, the management should be notified immediately, and corrective actions should be agreed with management and taken without delay. Other temporary measures (e.g. mobile detection systems) may need to be installed to compensate for defective criticality detection and alarm systems.

Relevant personnel should be given advance notice of the testing of subsystems of the alarm system and of any periods of time during which the system will be taken out of service. Operating rules should define the compensatory measures to be taken when the system is out of service.

Records of the tests (e.g. of the response of instruments and of the entire alarm system) should be maintained in accordance with approved quality assurance plans as part of the overall management system. (see paras 2.17–2.40).

Further guidance on criticality detection and alarm systems is provided in Ref. [50].
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Annex

RELEVANT LITERATURE

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Standards
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**Hand Calculation Methods**


**Computational Methods**


**Training and Education**


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- Module 4: Neutron Scattering and Moderation (PDF)
- Module 5: Criticality Safety Limits (PDF)
- Module 6: Introduction to Diffusion Theory (PDF)
- Module 7: Introduction to the Monte Carlo Method (PDF)
- Module 8: Hand Calculation Methods – Part I (PDF)
- Module 9: Hand Calculation Methods – Part 2
- Module 10: Criticality Safety in Material Processing Operations – Part 1 (PDF)
Module 11: Criticality Safety in Material Processing Operations — Part 2 (PDF)

Module 12: Preparation of Nuclear Criticality Safety Evaluations (PDF)

Module 13: Measurement and Development of Cross Section Sets (PDF)


Module 15: Fundamentals of Criticality Safety for Non-material Handlers (web based interactive training course)

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— Module 3: The Fission Chain Reaction (PDF)

— Module 4: Neutron Scattering and Moderation (PDF)

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— Module 13: Measurement and Development of Cross Section Sets (PDF)


— Module 15: Fundamentals of Criticality Safety for Non-material Handlers (web based interactive training course)

— Module 16: Burnup Credit for Criticality Safety Analysis of Commercial Spent Nuclear Fuel (PDF)

US Department of Energy Nuclear Criticality Safety Program Oak Ridge Critical Experiment Facility History Videos


Chapter 4: Facility Description http://ncsp.llnl.gov/flv/ORCEF1chapter4.html

Chapter 5: Characteristic Experimental Programs http://ncsp.llnl.gov/flv/ORCEF1chapter5.html


Chapter 7: Operational Safety Experiments and Analysis http://ncsp.llnl.gov/flv/ORCEF1chapter7.html

Chapter 8: Additional ORCEF Experimentalists http://ncsp.llnl.gov/flv/ORCEF1chapter8.html


Chapter 10: Sponsor and Credit http://ncsp.llnl.gov/flv/ORCEF1chapter10.html

Operational Experience and Accidents and Incidents

— Chapter 1: Early History of Criticality Experiments https://ncsp.llnl.gov/videos/ORCEF1Chapter1.mp4


— Chapter 4: Facility Description https://ncsp.llnl.gov/videos/ORCEF1Chapter4.mp4

— Chapter 5: Characteristic Experimental Programs https://ncsp.llnl.gov/videos/ORCEF1Chapter5.mp4


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— Chapter 8: Additional ORCEF Experimentalists https://ncsp.llnl.gov/videos/ORCEF1Chapter8.mp4

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